

# **TECHNICAL MEMORANDUM**

Project No. 1531406

DATE March 29, 2019

TO Renee Cipriano Schiff Hardin LLP

CC Ameren Missouri, Haley and Aldrich

**FROM** Golder Associates – Jeffrey Ingram, RG, Joanna Moreno, PH (GW)

# GROUNDWATER AND GEOCHEMICAL MODELING SUMMARY UPDATES FOR THE RUSH ISLAND ENERGY CENTER CORRECTIVE MEASURES ASSESSMENT

# 1.0 INTRODUCTION

Golder Associates Inc. (Golder) is pleased to submit this Technical Memorandum summarizing updated modeling and investigation results. In January of 2019 Golder submitted a detailed modeling Technical Memorandum entitled "*Groundwater and Geochemical Modeling Summary for Ameren Rush Island Energy Center Corrective Measures Assessment*". This current Technical Memorandum provides modeling and investigation updates for the January 2019 Technical Memorandum (Golder 2019a) based on comments and requests from Schiff Hardin, Ameren Missouri (Ameren), and Haley and Aldrich.

# 2.0 GROUNDWATER FLOW MODEL

# 2.1 Closure Scenario Groundwater Model Predictions

The calibrated model described in the Golder (2019a) Technical Memorandum was used to predict flow from the RCPA, flow rates in the alluvium, flows to/from the river, and to optimize recovery well placement and pumping rates for alternative closure scenarios. These scenarios are similar to those in the 2019 Golder report, however, these scenarios use a 18-inch thick  $1 \times 10^{-7}$  centimeter per second (cm/s) Cap with a 6-inch soil cover resulting in 1-inch per year infiltration, whereas the previous report detailed model runs using a  $1 \times 10^{-6}$  cm/s Cap of the same thickness resulting in 7 inches per year of infiltration to the RCPA. The scenarios modeled are summarized below in Table 1 and Figures 1-6.

Table 1: Summary	v of Steady-Sta	ate Groundwater	Model Predictio	ns for Future	Scenarios
Table 1. Summar	y of Steauy-Sta		would reductio		ocenarios

Future Prediction Model Scenario	Reference Figure	Mississippi River Stage (ft amsl)	Number of Wells	Well Pumping Rate (gpm)	Total Pumping Rate (gpm)	Slurry Wall?	Inward Hydraulic Gradient from Mississippi River toward the RCPA?
RCPA Cap of 18-inch thick 1 x 10 <sup>-7</sup> cm/s with a 6-inch soil cover (RCPA Cap)	Figure 1	366				No	No

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RCPA Cap, Hydraulic Containment with Pumping Wells #1	Figure 2	366	6	2.8	16.8	No	Yes
RCPA Cap, Hydraulic Containment with Pumping Wells #2	Figure 3	366	6	1.6	9.6	No	No
RCPA Cap, Hydraulic Containment with Pumping Wells #3	Figure 4	374.2	6	3.5	21.0	No	Yes
RCPA Cap, Hydraulic Containment with Slurry Wall and Pumping Wells #1	Figure 5	366	6	2.3	13.8	Yes	Yes
RCPA Cap, Hydraulic Containment with Slurry Wall and Pumping Wells #2	Figure 6	374.2	6	2.8	16.8	Yes	Yes

## Notes:

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1) cm/s = centimeters per second.

2) ft amsl = feet above mean sea level.

3) gpm = gallons per minute.

4) In all future model scenarios, the RCPA was modeled as drained, inactive, and capped with RCPA recharge of 1-inch/year based on Haley & Aldrich 2018 HELP model net infiltration prediction for 1 x 10<sup>-7</sup> cm/s soil cover.
5) Mississippi River stage of 366 ft amsl is the steady-state equivalent river stage and 374.2 ft amsl is the long-term average river stage calculated from 1983 to 2017.

6) Hydraulic head control was predicted using proposed pumping wells placed at approximately 1000 foot spacing. Each proposed well is simulated to screen very shallow alluvium to the base of the intermediate alluvium.

7) RCPA hydraulic containment was evaluated using predicted flow velocity vectors and predicted pumping well capture of particles distributed along the outside edge of the RCPA in each model ash layer (Golder 2019).
8) The proposed slurry wall was modeled as constructed along the east side of the RCPA from the very shallow alluvium to the base of the deep alluvium/top of bedrock, 2 feet thick, and a hydraulic conductivity of 1 x 10<sup>-6</sup> cm/s.

The reduction in pumping rates between the scenarios with a 1 x  $10^{-6}$  cap in the Golder 2019 report and those displayed above with a 1 x  $10^{-7}$  cap are due to the reduction in infiltration through the cap. Based on the Haley and Aldrich (2018) HELP model, there is a reduction from 7-inches per year (1 x  $10^{-6}$  cap) to 1-inch per year (1 x  $10^{-7}$  cap). This 86% reduction in infiltration to the RCPA reduces the pumping rates required by 70-85%.

# 2.2 Model Estimates of Flow Around the RCPA Based on Ash K

Model estimates of groundwater flow into and around the RCPA varies with the assumed hydraulic conductivity of the RCPA ash. The horizontal hydraulic conductivity of the RCPA ash was estimated to be 3.0 x 10<sup>-3</sup> cm/sec based on slug testing results and the model calibration process (Golder 2019a). Table 2 below displays the change in flow into and around the RCPA based on different ash hydraulic conductivity values. As shown on Table 2, if the horizontal conductivity of the ash is decreased by an order of magnitude, the model simulations show that there would be no flow into the RCPA from the alluvial aquifer and that all groundwater flowing from

upgradient of the RCPA would preferentially flow around the RCPA. Example particle pathways that display this preferential flow pattern around the RCPA are provided in Figure 7. No upgradient groundwater is simulated to flow into the RCPA with the lower horizontal conductivity values because the lower conductivity ash causes a small amount of mounding in the RCPA (estimated to be 0.05 to 0.3 feet).

Horizontal	Vertical						
Hydraulic	Hydraulic	Flow	Flow				
Conductivity	Conductivity	Around the	Through the	Percent Flow	Percent Flow		
(Kx,Ky) of RCPA Ash	(Kz) of RCPA Ash	RCPA	RCPA	Around RCPA	Through the RCPA		
Centimeter p	er Second	Gallons	per Minute	Percent			
3.0 x 10 <sup>-3</sup>	9.8 x 10 <sup>-5</sup>	3.6	0.2	94.7%	5.3%		
3.0 x 10 <sup>-4</sup>	9.8 x 10 <sup>-5</sup>	4.1	0.0	100.0%	0.0%		
3.0 x 10 <sup>-5</sup>	9.8 x 10 <sup>-5</sup>	4.2	0.0	100.0%	0.0%		

Table 2. Model	Estimates	of Flow	Around ve	Into the	RCPA	<b>Based</b> on	∆sh	Conductivity
	Lotimates					Daseu on	<b>A</b> SII	Conductivity

### Notes:

1) In all future model scenarios, the RCPA was modeled as drained, inactive, and with the RCPA cap resulting in an infiltration rate of 1-inch/year to the RCPA based on Haley & Aldrich 2018 HELP model net infiltration prediction for  $1 \times 10^{-7}$  cm/s cap.

2) Mississippi River stage of 366 ft amsl is the steady-state equivalent river stage used in each of the model scenarios.

# 3.0 GEOCHEMICAL MODELING UPDATES

The PHAST geochemical model used in the Golder 2019 Technical Memorandum was updated to incorporate the use of an 18-inch thick 1 x  $10^{-7}$  cap with 6-inches of soil cover instead of a 1 x  $10^{-6}$  cap of the same thickness. Figures 8-14 compare the concentration over time between a 1 x  $10^{-6}$  and a 1 x  $10^{-7}$  cap at locations described in the Golder 2019 report (Golder 2019a).

# 4.0 WATER LEVELS

Periodic water levels have been collected in the pore-water within the RCPA and in the alluvial aquifer around the RCPA. Figure 15 displays the locations of where groundwater and pore-water elevation measurements were obtained and the results from these measurements are provided in Table 3.

## Tables:

Table 1 - Summary of Steady-State Groundwater Flow Model Predictions for Future Scenarios

Table 2 - Model Estimates of Flow Around vs Into the RCPA Based on Ash Conductivity

Table 3 - Summary of Groundwater Elevation Measurements

## Figures:

Figure 1 - Steady-State Groundwater Model Predictions - Historical (No Cap) and Future (With Cap) Conditions With Forward Particle Flow Paths



Figure 2 - Steady-State Groundwater Model Predictions - Capped RCPA With Six Proposed Pumping Wells, River Stage 366 Feet AMSL

Figure 3 - Steady-State Groundwater Model Predictions - Capped RCPA with Six Proposed Pumping Wells, River Stage 366 Feet AMSL, No Inward HYD Gradient

Figure 4 - Steady-State Groundwater Model Predictions - Capped RCPA with Six Proposed Pumping Wells, Long-Term Ave River Stage 374.2 Feet AMSL

Figure 5 - Steady-State Groundwater Model Predictions - Capped RCPA with Slurry Wall and Proposed Pumping Wells, River Stage 366 Feet AMSL

Figure 6 - Steady-State Groundwater Model Predictions - Capped RCPA with Slurry Wall and Proposed Pumping Wells, Long-Term Average River Stage

- Figure 7 Particle Flow Paths Around the RCPA
- Figure 8 Time Series Plot Average Concentrations at Location 1
- Figure 9 Time Series Plot Average Concentrations at Location 2
- Figure 10 Time Series Plot Average Concentrations at Location 3

Figure 11 – Time Series Plot – Average Concentrations at Location 4

Figure 12 – Time Series Plot – Average Concentrations at Location 5

Figure 13 – Time Series Plot – Average Concentrations at Location 6

Figure 14 – Time Series Plot – Average Concentrations at Location 7

Figure 15 – Groundwater Elevation Measurement Location Map

### References

Golder 2019a. Groundwater and Geochemical Modeling Summary for the Rush Island Energy Center Corrective Measures Assessment. Technical Memorandum, January 2019.

Haley and Aldrich 2018. HELP Model results for different cap scenarios.

# Tables



## Table 3 Summary of Groundwater Elevation Monitoring Results **Rush Island Energy Center** Jefferson County, Missouri

Well ID	Loca	ition	Top of Casing	Ground Surface Elevation	Ground Wa Measur 1/10	ter Elevation ements - /2018	Ground Wat Measur 4/2/	ter Elevation ements - '2018	Ground Wat Measure 5/24,	ter Elevation ements - /2018	Ground Wat Measur 6/22	ter Elevation ements - /2018	Ground Wat Measur 7/19	ter Elevation ements - /2018	Ground Wa Measur 8/20	ter Elevation ements - /2018	Ground Wat Measure 9/25/	er Elevation ements - '2018	Ground Wat Measure 11/1,	er Elevation ements - /2018	Ground Wat Measure 12/5/	ter Elevation ements - /2018	Ground Wat Measure 1/4/	er Elevation ements - 2019	Ground Wate Measure 2/25/	er Elevation ments - '2019
	Northing	Easting	FT MSL <sup>2</sup>	FT MSL <sup>2</sup>	DTW <sup>3</sup>	GWE <sup>4</sup>	DTW <sup>3</sup>	GWE <sup>4</sup>	DTW <sup>3</sup>	GWE <sup>4</sup>	DTW <sup>3</sup>	GWE <sup>4</sup>	DTW <sup>3</sup>	GWE <sup>4</sup>	DTW <sup>3</sup>	GWE <sup>4</sup>	DTW <sup>3</sup>	GWE <sup>4</sup>	DTW <sup>3</sup>	GWE <sup>4</sup>	DTW <sup>3</sup>	GWE <sup>4</sup>	DTW <sup>3</sup>	GWE <sup>4</sup>	DTW <sup>3</sup>	GWE <sup>4</sup>
												CCR RULE N	IONITORING V	VELLS												
R-MW-1	835,384.2	889,832.5	395.52	393.50	35.91	359.61	15.40	380.12	11.53	383.99	17.45	378.07	17.03	378.49	24.98	370.54	17.35	378.17	11.61	383.91	11.81	383.71	10.07	385.45	16.19	379.33
R-MW-2	834,261.5	890,364.1	393.87	391.70	33.42	360.45	13.87	380.00	9.96	383.91	15.95	377.92	15.73	378.14	23.53	370.34	16.07	377.80	10.31	383.56	10.19	383.68	8.49	385.38	14.91	378.96
R-MW-3	833,178.4	890,892.7	391.38	389.20	31.38	360.00	11.55	379.83	7.53	383.85	13.60	377.78	13.53	377.85	21.30	370.08	13.87	377.51	8.04	383.34	7.79	383.59	6.08	385.30	12.19	379.19
R-MW-4	831,647.5	890,830.5	392.78	390.80	32.30	360.48	12.89	379.89	9.10	383.68	14.98	377.80	14.64	378.14	22.35	370.43	12.94	379.84	9.29	383.49	9.71	383.07	7.51	385.27	13.63	379.15
R-MW-5	831,994.9	889,984.5	390.36	388.00	28.93	361.43	10.86	379.50	6.40	383.96	12.25	378.11	11.78	378.58	19.27	371.09	12.06	378.30	6.54	383.82	7.24	383.12	4.87	385.49	10.83	379.53
R-MW-6	833,111.0	888,977.0	402.71	401.10	40.26	362.45	20.84	381.87	18.27	384.44	24.50	378.21	24.29	378.42	30.35	372.36	23.56	379.15	18.29	384.42	19.46	383.25	17.11	385.60	21.62	381.09
R-MW-7	834,476.8	888,483.3	407.95	406.10	45.28	362.67	27.62	380.33	24.33	383.62	29.64	378.31	28.23	379.72	36.48	371.47	28.33	379.62	23.48	384.47	25.23	382.72	22.82	385.13	28.89	379.06
R-MW-B1	837,602.1	887,903.9	411.61	409.60	51.69	359.92	31.50	380.11	28.01	383.60	33.50	378.11	31.81	379.80	40.51	371.10	32.01	379.60	27.21	384.40	28.69	382.92	26.24	385.37	32.10	379.51
R-MW-B2	837,801.7	885,337.2	397.85	395.90	35.44	362.41	17.80	380.05	14.55	383.30	19.59	378.26	17.10	380.75	29.50	368.35	16.69	381.16	12.36	385.49	15.07	382.78	12.23	385.62	17.09	380.76
				-	-					-	NA	ATURE AND EXT	TENT MONITOR	RING WELLS					-			-				
R-P-01S	831,422.3	890,858.9	387.62	385.69	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.74	383.88	4.68	382.94	2.24	385.38	<u> </u>	-
R-P-03D	831,686.3	890,369.8	391.65	389.34	-	-	-	-	7.81	383.84	13.50	378.15	13.05	378.60	20.61	371.04	13.33	378.32	7.75	383.90	8.36	383.29	6.04	385.61	<u> </u>	-
R-P-03S	831,690.9	890,352.1	391.68	389.48	-	-	-	-	7.80	383.88	13.50	378.18	13.01	378.67	20.52	371.16	12.52	379.16	7.65	384.03	8.54	383.14	6.10	385.58		-
R-P-05I	832,295.4	889,756.1	390.07	387.87	-	-	-	-	5.83	384.24	11.69	378.38	11.16	378.91	18.63	371.44	11.41	378.66	5.95	384.12	6.67	383.40	4.31	385.76		-
R-P-05S	832,317.6	889,749.7	392.50	390.05	-	-	-	-	8.25	384.25	14.09	378.41	13.71	378.79	20.87	371.63	12.81	379.69	8.34	384.16	9.12	383.38	6.69	385.81		-
R-P-08D	833,687.5	888,715.1	404.61	401.77	-	-	-	-	20.58	384.03	26.25	378.36	25.07	379.54	32.97	371.64	25.22	379.39	20.04	384.57	21.61	383.00	19.01	385.60		
R-P-08S	833,692.6	888,711.1	404.79	402.03	-	-	-	-	20.74	384.05	25.87	378.92	23.69	381.10	30.66	374.13	22.65	382.14	18.33	386.46	21.95	382.84	19.57	385.22		
R-P-10S	834,545.1	888,099.0	407.23	404.83	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22.16	385.07	24.39	382.84	21.37	385.86		-
R-P-13D	834,992.6	889,105.8	410.40	408.52	-	-	-	-	26.59	383.81	32.25	378.15	31.21	379.19	39.42	370.98	31.46	378.94	26.21	384.19	27.24	383.16	25.04	385.36		
R-P-13I	834,995.2	889,110.6	410.52	408.57	-	-	-	-	26.63	383.89	32.30	378.22	31.25	379.27	39.42	371.10	31.36	379.16	26.11	384.41	27.33	383.19	25.08	385.44		-
R-P-13S	835,005.5	889,108.3	411.62	409.25	-	-	-	-	27.77	383.85	33.40	378.22	32.26	379.36	40.47	371.15	32.44	379.18	27.26	384.36	28.46	383.16	26.28	385.34		-
R-P-17D	834,718.8	890,158.3	395.56	392.62	-	-	-	-	11.43	384.13	17.44	378.12	17.19	378.37	25.03	370.53	17.51	378.05	11.77	383.79	11.61	383.95	9.96	385.60		
R-P-17I	834,744.2	890,148.9	394.86	392.53	-	-	-	-	12.06	382.80	16.72	378.14	16.44	378.42	24.28	370.58	14.16	380.70	11.03	383.83	11.00	383.86	9.29	385.57		-
R-P-17S	834,736.7	890,152.8	394.65	392.49	-	-	-	-	10.71	383.94	15.75	378.90	14.24	380.41	18.65	376.00	16.79	377.86	6.96	387.69	10.96	383.69	10.48	384.17		-
R-P-19D	833,915.6	890,552.2	392.08	390.31	-	-	-	-	8.46	383.62	14.50	377.58	14.32	377.76	22.10	369.98	14.68	377.40	8.89	383.19	9.70	382.38	7.01	385.07		-
R-P-19I	833,911.3	890,550.6	392.75	390.24	-	-	-	-	8.11	384.64	14.14	378.61	13.94	378.81	21.72	371.03	14.30	378.45	8.51	384.24	8.37	384.38	6.66	386.09		-
R-P-19S	833,919.0	890,546.4	393.31	390.58	-	-	-	-	9.67	383.64	15.32	377.99	14.86	378.45	22.68	370.63	15.21	378.10	9.10	384.21	9.94	383.37	8.15	385.16	<u> </u>	
R-P-21D	832,902.9	891,031.2	393.39	391.04	-	-	-	-	9.39	384.00	15.48	377.91	15.38	378.01	23.16	370.23	15.73	377.66	9.93	383.46	9.63	383.76	7.89	385.50	<u> </u>	
R-P-211	832,904.2	891,027.0	393.53	391.19	-	-	-	-	9.43	384.10	15.51	378.02	15.41	378.12	23.20	370.33	15.74	377.79	9.95	383.58	9.68	383.85	7.94	385.59	<u>↓ - </u> ↓	
R-P-21S	832,898.0	891,024.7	393.87	391.45	-	-	-	-	10.24	383.63	16.07	377.80	16.77	377.10	23.48	370.39	16.02	377.85	9.91	383.96	10.59	383.28	8.73	385.14	<u> </u>	
R-P-22D	832,278.2	891,018.7	393.76	391.63	-	-	-	-	9.86	383.90	15.84	377.92	15.61	378.15	23.46	370.30	15.93	377.83	10.26	383.50	10.25	383.51	8.33	385.43	<u>↓ ·</u> ↓	
R-P-22I	832,272.1	891,018.0	393.52	391.59	-	-	-	-	9.66	383.86	15.67	377.85	15.44	378.08	23.27	370.25	15.75	3/7.77	10.03	383.49	10.11	383.41	8.15	385.37		-
R-P-22S	832,277.0	891,007.6	394.30	392.15	-	-	-	-	10.46	383.84	16.39	377.91	15.93	378.37	23.89	370.41	16.19	378.11	10.60	383.70	11.12	383.18	9.01	385.29		-
R-P-29D	837,804.9	885,389.1	398.27	396.23	-	-	-	-	14.73	383.54	19.76	378.51	17.28	380.99	25.68	372.59	16.86	381.41	12.54	385.73	15.23	383.04	12.39	385.88	<u>↓ ·</u> ↓	
R-P-29S	837,797.9	885,383.8	399.11	397.02	-	-	-	-	16.42	382.69	20.52	378.59	17.63	381.48	24.35	374.76	16.72	382.39	13.36	385.75	16.08	383.03	13.65	385.46		-
R-P-305	836,606.9	889,007.8	407.75	407.98	-	-	-	-	-	-	-	-	-	-	-	-	-	-	25.20	382.55	24.53	383.22	22.60	385.15		-
R-P-31S	835,629.4	887,488.1	408.68	406.08	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22.31	386.37	25.38	383.30	22.48	386.20	<u> </u>	-
						1		1	_		-	PORE-WATER	MONITORING	WELLS		1			<b>I</b>							
R-P-275	834,319.5	888,680.9	413.23	410.33	-	-	-	-	-	-	-	-	-	-		-	-	-	14.91	398.32	18.87	394.36	18.09	395.14	<u> </u>	-
R-P-285	834,/88.3	889,594.3	413.34	410.86	-	-	-	-	-	-	-	-	-	-	-	-	-	-	21.35	391.99	23.80	389.54	25.51	387.83		-
Pond Gauge	890854*	832689*	NA	NA	NA	388.5	NA	398.0	NA	398.0	NA	396.0	NA	394.0	NA	395.0	NA	396.0	NA	394.0	NA	394.5	NA	394.0	NA	390.5
Mississippi River <sup>7</sup>	888823*	837705*	NA	NA	NA	361.20	NA	380.94	NA	385.38	NA	379.40	NA	379.41	NA	371.69	NA	379.08	NA	384.79	NA	385.29	NA	386.72	NA	380.56

Notes: 1.) \* - Mississippi River and Pond gauge location is estimated.

2.) MSL - Feet above mean sea level.

3.) DTW - Depth to water measured in feet below top of casing.

4.) GWE - Groundwater elevation measured in feet above mean sea level.

5.) Horizontal Datum: State Plane Coordinates NAD83 (2000) Missouri East Zone feet.

6.) Vertical Datum: NAVD88 feet.

7.) Mississippi River gage elevation provided by Ameren8.) NA - Not Applicable

9.) "-" - Ground water elevation measurement not collected.

Prepared By: EMS Checked by: JAP Reveiwed By: MNH

# Figures









### Particle Trace Colors



#### Proposed Pumping Wells for Hydraulic Containment

PW-01 Proposed Pumping Well

6 Proposed Pumping Wells Approx. 1000 foot spacing Screened from Very Shallow Alluvium to Intermediate Alluvium Upward Vertical Hydraulic Gradient predicted in Deep Alluvium near each well

Predicted hydraulic containment of RCPA particles and inward hydraulic gradient from the Mississippi River toward the RCPA maintained based on:

Each Well Pumping Rate = **2.8 gpm** Total Pumping Rate = **16.8 gpm** 

### Model Boundary Condition Cells



NOTE(S)

1. Steady-state groundwater model predictions.

2. Mississippi River at steady-state equivalent river stage of 366 feet above mean sea level.

 Particles distributed along the outside edge of the RCPA in each model ash layer. See Figure Golder 2019 Technical Memorandum for details on starting particle locations.
 Cap model includes 1.0 inch/year recharge to the RCPA based on Haley & Aldrich 2018 HELP model net infiltration prediction for 1 x 10<sup>-7</sup> cm/s soil cover.

# AMEREN MISSOURI RUSH ISLAND ENERGY CENTER



GROUNDWATER MONITORING PROGRAM

1531406

STEADY-STATE GROUNDWATER MODEL PREDICTIONS CAPPED RCPA WITH SIX PROPOSED PUMPING WELLS, RIVER STAGE 366 FEET AMSL PROJECT NO. REV.

CONSULTANT





AMEREN\_00003983

Α

FIGURE





#### **Particle Trace Colors**

 RCPA or Shallow Alluvium
 RCPA or Intermediate Alluvium
 Intermediate/Deep Alluvium

#### **Proposed Pumping Wells for** Hydraulic Containment

**PW-01** Proposed Pumping Well

6 Proposed Pumping Wells Approx. 1000 foot spacing Screened from Very Shallow Alluvium to Intermediate Alluvium Upward Vertical Hydraulic Gradient predicted in Deep Alluvium near each well

Predicted hydraulic containment of RCPA particles based on: Each Well Pumping Rate = 1.6 gpm Total Pumping Rate = **9.6 gpm** 

Inward hydraulic gradient from the Mississippi River toward the RCPA not maintained

### Model Boundary Condition Cells



NOTE(S)

1. Steady-state groundwater model predictions. 2. Mississippi River at steady-state equivalent river stage of 366 feet above mean sea level. 3. Particles distributed along the outside edge of the RCPA in each model ash layer. See Golder (2019) Technical Memorandum for details on starting particle locations. 4. Cap model includes 1.0 inchvjear recharge to the RCPA based on Haley & Aldrich 2018 HELP model net infiltration prediction for 1 x  $10^7$  cm/s soil cover.

# AMEREN MISSOURI RUSH ISLAND ENERGY CENTER

GOLDER



JSI

RT

JM

MNH

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GROUNDWATER MONITORING PROGRAM



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FIGURE

3







### Particle Trace Colors

 RCPA or Shallow Alluvium
 RCPA or Intermediate Alluvium
 Intermediate/Deep Alluvium

#### **Proposed Pumping Wells for** Hydraulic Containment

**PW-01** Proposed Pumping Well

6 Proposed Pumping Wells Approx. 1000 foot spacing Screened from Very Shallow Alluvium to Intermediate Alluvium Upward Vertical Hydraulic Gradient predicted in Deep Alluvium near each well

Predicted hydraulic containment of RCPA particles and inward hydraulic gradient from the Mississippi River toward the RCPA maintained based on.

Each Well Pumping Rate = 3.5 gpm Total Pumping Rate = 21.0 gpm

### Model Boundary Condition Cells



NOTE(S)

1. Steady-state groundwater model predictions.

2. Mississippi River at long-term average river stage of 374.2 feet above mean sea level.

3. Particles distributed along the outside edge of the RCPA in each model ash layer. See Golder (2019) Technical Memorandum for details on starting particle locations. 4. Cap model includes 1.0 inches/year recharge to the RCPA based on Haley & Aldrich 2018 HELP model net infiltration prediction for 1 x 10<sup>7</sup> cm/s soil cover.

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#### Particle Trace Colors



#### **Proposed Pumping Wells for Hydraulic Containment**

**PW-01** Proposed Pumping Well

6 Proposed Pumping Wells Approx. 1000 foot spacing Screened from Very Shallow Alluvium to Intermediate Alluvium Upward Vertical Hydraulic Gradient predicted in Deep Alluvium near each well

Predicted hydraulic containment of RCPA particles and inward hydraulic gradient from the Mississippi River toward the RCPA maintained based on:

Proposed Slurry Wall Each Well Pumping Rate = 2.3 gpm Total Pumping Rate = 13.8 gpm

#### Model Boundary Condition Cells



River

Proposed Slurry Wall

Constructed from Very Shallow Alluvium to Deep Alluvium/ Top of Bedrock 2 foot thick wall Hydraulic Conductivity = 1 x10<sup>-6</sup> cm/s

NOTE(S)

1. Steady-state groundwater model predictions.

2. Mississippi River at steady-state equivalent river stage of 366 feet above mean sea level.

3. Particles distributed along the outside edge of the RCPA in each model ash layer. See Golder (2019) Technical Memorandum for details on starting particle locations. 4. Cap model includes 1.0 inches/year recharge to the RCPA based on Haley & Aldrich 2018 HELP model net infiltration prediction for 1 x 10<sup>7</sup> cm/s soil cover.

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#### Particle Trace Colors



#### **Proposed Pumping Wells for Hydraulic Containment**

**PW-01** Proposed Pumping Well

6 Proposed Pumping Wells Approx. 1000 foot spacing Screened from Very Shallow Alluvium to Intermediate Alluvium Upward Vertical Hydraulic Gradient predicted in Deep Alluvium near each well

Predicted hydraulic containment of RCPA particles and inward hydraulic gradient from the Mississippi River toward the RCPA maintained based on:

Proposed Slurry Wall Each Well Pumping Rate = 2.8 gpm Total Pumping Rate = 16.8 gpm

#### Model Boundary Condition Cells



River

Proposed Slurry Wall Constructed from Very Shallow Alluvium to Deep Alluvium/ Top of Bedrock 2 foot thick wall Hydraulic Conductivity = 1 x10<sup>-6</sup> cm/s

NOTE(S)

1. Steady-state groundwater model predictions.

2. Mississippi River at long-term average river stage of 374.2 feet above mean sea level.

3. Particles distributed along the outside edge of the RCPA in each model ash layer. See Golder (2019) Technical Memorandum for details on starting particle locations. 4. Cap model includes 1.0 inches/year recharge to the RCPA based on Haley & Aldrich 2018 HELP model net infiltration prediction for 1 x 10<sup>7</sup> cm/s soil cover.

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1) In this steady state scenario, the RCPA was modeled as drained, inactive, and capped with a infiltration rate to the RCPA of 1-inch/year based on Haley & Aldrich 2018 HELP model.

2) A Mississippi River stage of 366 ft amsl is the steady-state equivalent river stage used.

3) Particles display forward tracking with starting points at the top of layer 2 (Shallow Alluvial Aquifer).

4) Aerial view displays Layer 2 (Shallow Alluvial Aquifer).

5) Model displays results using the ash conductivities displayed in the Golder 2019 Technical memorandum with a kx,ky value of 3 x 10<sup>-3</sup> centimeters per second and a kz value of 9.8 x 10<sup>-4</sup> centimeters per second.



















#### LEGEND

- 📕 📕 🦉 Rush Island Energy Center Property Boundary
  - RCPA Surface Impoundment
  - $\oplus$ 
    - RCPA CCR Rule Monitoring Well Location
  - Existing Monitoring Well Used for Nature and Extent JANUARY 2012.  $\otimes$ 
    - Pore-water Monitoring Well

NOTES 1. ALL LOCATIONS AND BOUNDARIES ARE APPROXIMATE. SOME PIEZOMETER LOCATIONS OFFSET FOR CLARITY PURPOSES.

#### REFERENCE

1.) AMEREN MISSOURI RUSH ISLAND ENERGY CENTER, RUSH ISLAND PROPERTY CONTROL MAP,

2.) NRT 2014, NATURAL RESOURCE TECHNOLOGY, RUSH ISLAND IMPOUNDMENT POND CLOSURE GROUNDWATER MONITORING AND SAMPLING PLAN, MARCH 4, 2014.

3.) COORDINATE SYSTEM: NAD 1983 STATEPLANE MISSOURI EAST FIPS 2401 FEET.

250 500 750 1,000 0 E Feet

#### CLIENT AMEREN MISSOURI RUSH ISLAND ENERGY CENTER



#### PROJE

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# GROUNDWATER ELEVATION MEASUREMENT LOCATION MAP

