Project No. 1531406

# **TECHNICAL MEMORANDUM**

DATE March 15, 2019

- TO Renee Cipriano Schiff Hardin LLP
- CC Ameren Missouri
- **FROM** Golder Associates Jeff Ingram, RG, Mark Haddock PE, RG

EMAIL Mark\_Haddock@golder.com

### GROUNDWATER AND GEOCHEMICAL MODELING SUMMARY FOR AMEREN SIOUX ENERGY CENTER CORRECTIVE MEASURES ASSESSMENT

### 1.0 INTRODUCTION

Golder Associates Inc. (Golder) is pleased to submit this Technical Memorandum summarizing modeling results under various closure scenarios at the Ameren Missouri (Ameren) Sioux Energy Center (SEC) in St. Charles County Missouri. As part of the SEC Corrective Measures Assessment (CMA), the fate and transport of metals under various closure scenarios were investigated through modeling and this memo summarizes these tasks conducted in support of the CMA.

### 2.0 GROUNDWATER FLOW MODEL

### 2.1 Introduction

Golder has developed a groundwater flow model for the SEC. There have been many groundwater samples, surface water samples, and groundwater elevation measurements collected at the SEC and these sampling locations which were used to generate the model are shown in Figure 1. The area covered by the groundwater flow model is shown in Figure 2. The purpose of this groundwater model summary is to document model setup, calibration and prediction results, and related data. This summary is being provided for the use of Ameren, Haley & Aldrich, and Golder staff familiar with the site and the model and is not intended as a detailed report for regulatory review or other purposes.

### 2.2 General Setting

The groundwater modeling is focused on modeling flow and transport in the alluvium underlying the SEC and bounded by the adjacent reach of the Mississippi and Missouri Rivers (Figure 2).

### 2.3 Groundwater Modeling Objectives

The objectives of the modeling analysis are to:

- Synthesize the most recent hydrogeologic data into an integrated conceptual and numerical framework for evaluating remedial strategies at the Site
- Use the groundwater model to predict and compare groundwater conditions resulting from different remedial alternatives for the SCPA
- Use the groundwater model to predict future Molybdenum concentrations after capping and closing the SCPA.

## 2.4 TECHNICAL APPROACH

The hydrogeologic conceptual model and model framework are described in this section.

### 2.4.1 Data Sources

- 1. The primary data sources used were as follows:
- Golder (2017a, 2017b, 2017c, 2017d, 2018a, 2018b, 2018c, 2018d, 2018e, 2019a, 2019b, 2019c, 2019d, 2019e) general hydrogeology, geology, aquifer slug test results, potentiometric maps, water quality data, aerial photographs, ash pile geometry.
- 3. Haley & Aldrich (2018) surface water data.
- 4. Gredell (2006, 2009) general hydrogeology, geology, aquifer slug testing results, potentiometric maps, water quality data, groundwater elevation measurements.

- 5. United States Geological Survey (USGS): river gauge data.
- 6. Rietz & Jens, Inc., and Gredell Engineering Resources (2014) Utility Waste Landfill design.
- 7. Electric Power Research Institute (EPRI 1998), SCPA water balance, water quality data, ash pile geometry.

A summary of the model input data derived from these and other sources is provided in Table 1.

Parameter	Reported Range	Model Values	Data Source
Groundwater Elevations	413.2 to 435.5 ft MSL	413.8 to 433.0 ft MSL	Golder 2017 (a-d), 2018 (a-d), and 2019 (a-e), Gredell 2006 and 2009
Missouri and Mississippi River Elevations ( ft MSL)	<u>USGS Gauges</u> St. Charles Gauge – 417.08 - 453.15 Grafton Gauge – 417.94 – 441.96 Alton Gauge – 407.83 – 437.76 St. Louis Gauge – 374.26 – 429.05	Calculated Model Values (Average Annual Levels at Plant) Missouri River – 413.2 – 425.3 Mississippi River – 417.5 - 420.7	USGS Gauges 06935956, 05587450, 05587541, 07010000
	Saturated Lay	/er Thickness	
Layer 1		0 to 36 feet	
Layer 2		25 to 32 feet	Laver thickness based on
Layer 3	ΝΔ	6 to 27 feet	Boring Logs (Golder
Layer 4		23 feet	(a-d), Golder 2019 (a-e),
Layer 5		25 feet	Gredell 2006,
Layer 6		65 feet	
	Infiltrat	ion rate	
SCPA Pond - Active	0.04	From 0.015 to 0.03 ft/day (66-131 in/yr)	EPRI 1998, Calibrated Values
SCPA Pond Capped - 1.0E-7cm/sec Cap, 1.5 feet thick	NA	0.00023 ft/day (1.0 in/yr)	Data from Rush Island (Golder, 2019), Haley and Aldrich 2018

### Table 1: Model Import Data Ranges

Non-ponded areas natural recharge) 2 to 22 in/yr 0.00059 ft/day (2.5		Owuor et al., 2016, USGS 2001 and 2010, Calibrated Values	
Horizontal Hydraulic Con	ductivity (Kx, Ky) cm/sec	;	
1.0E-4 to 1.0E-6	9.9E-04	Fetter, C.W., 2001, Calibrated Values	
Minimum: 5.6E-03			
Maximum: 2.6E-02	2.6E-02	Golder 2017(a-d), Calibrated Values	
Geomean: 1.6E-02			
Minimum: 8.8E-03			
Maximum: 4.0E-02	4.0E-02	Golder 2017(a-d), Calibrated Values	
Geomean: 1.8E-02			
Minimum: 2.1E-07		Golder 2018e, Calibrated Values	
Maximum: 4.9E-03	1.8E-04		
Minimum: 1.1E-05		Golder 2018e. Calibrated	
Maximum: 4.9E-03	1.8E-04	Values	
1.0E-02 to 1.0E-08	9.9E-07	Fetter, C.W., 2001, Calibrated Values	
1.0E-3 to 1.0E-9	2.7E-06	Fetter, C.W., 2001, Calibrated Values	
Other Pa	rameters		
0.16 to 0.46	0.25	Morris and Johnson (1967)	
	2 to 22 in/yr Horizontal Hydraulic Con 1.0E-4 to 1.0E-6 Minimum: 5.6E-03 Maximum: 2.6E-02 Geomean: 1.6E-02 Minimum: 8.8E-03 Maximum: 4.0E-02 Geomean: 1.8E-02 Minimum: 2.1E-07 Maximum: 4.9E-03 Minimum: 1.1E-05 Maximum: 4.9E-03 1.0E-02 to 1.0E-08 1.0E-3 to 1.0E-9 Other Pa 0.16 to 0.46	2 to 22 in/yr    0.00059 ft/day (2.5 in/yr)      Horizontal Hydraulic Conductivity (Kx, Ky) cm/sec      1.0E-4 to 1.0E-6    9.9E-04      Minimum: 5.6E-03    2.6E-02      Geomean: 1.6E-02    2.6E-02      Geomean: 1.6E-02    4.0E-02      Geomean: 1.8E-03    4.0E-02      Maximum: 2.1E-07    1.8E-04      Maximum: 4.9E-03    1.8E-04      Minimum: 1.1E-05    1.8E-04      Maximum: 4.9E-03    2.7E-06      Other Parameters      0.16 to 0.46    0.25	

Notes:

1) NA = Not applicable

2) ft MSL - feet above mean sea level

3) in/yr - inches per year

4) cm/sec - centimeters per second

5) SEC – Sioux Energy Center

6) ft/day - feet per day

## 2.5 Conceptual Model

The Site is located in the floodplain between the Mississippi and Missouri Rivers and lies on alluvial deposits associated with these rivers. The alluvial deposits comprise the surficial alluvial aquifer, which lies unconformably on top of bedrock and is typically 100 to 130 feet thick. Overall, this aquifer is described as a fining upwards sequence of stratified sands and gravels with varying amounts of silts and clays. Drilling in the alluvial aquifer identified different sub-units, including flood basin deposits, floodplain deposits, natural levee deposits, and channel deposits along with volumetrically less important loess deposits. Grain sizes of the alluvial deposits are highly variable.

Bedrock below the alluvial aquifer includes Mississippian-aged rocks of the Meramecian Series. Formations include primarily limestone, dolomite, and shale and are comprised of the Salem Formation, Warsaw Formation, and the Osagean aged Burlington-Keokuk Formation.

Groundwater generally flows from the higher water elevations of either of the Mississippi and Missouri Rivers towards the lower water elevation river with a slight component of west to east flow in the downriver direction. River elevations in both rivers change frequently and there is not a constant river with a higher elevation, therefore there are multiple directions of groundwater flow.

Hydraulic sources (inflows) consist primarily of recharge from precipitation, groundwater inflows from the west (up-river) to the east, inflows from the Mississippi and Missouri Rivers, and seepage from the SCPA. Hydraulic sinks (outflows) includes discharge to rivers.

### 2.6 Selection of Computer Code

The numerical computer code MODFLOW – developed by the United States Geological Survey (USGS) – was selected for much of this analysis because it is well suited to represent a wide range of hydrologic and hydrogeologic conditions, has been widely tested and accepted in the professional hydrology community and by regulatory agencies, and has been scrutinized closely in a number of legal proceedings over the past 20 years. In total, five software packages were used for the groundwater investigation:

- Groundwater flow: USGS software package MODFLOW (McDonald and Harbaugh 1988, Harbaugh and McDonald 1996, Harbaugh et al. 2000, Harbaugh 2005). MODFLOW-2005 was used in the analyses presented here.
- Groundwater transport: USGS software package MT3DMS (Zheng and Wang, 1999).
- Particle tracking: USGS software package MODPATH (Pollock 2012)
- Parameter estimation: PEST (Doherty 2010 and 2016)
- Graphical user interface: Groundwater Vistas (Environmental Simulations 2017, Rumbaugh and Rumbaugh 2011).

### 2.7 Groundwater Model Construction

The model grid was oriented to align with the SCPA and river bank with the primary flow direction of the Mississippi River (Figure 3). The gird sizes are uniform horizontally (100 ft by 100 ft) and vary with the geologic layer thicknesses and SCPA geometry in the vertical. The six layers modeled are shown in Figures 4 and 5 along with their hydraulic conductivities.

Model boundary conditions include: recharge at the ground surface and on the surface of the SCPA (Figure 6), river boundary conditions at the rivers, creeks, and small ponds (Figure 7), and general head boundary conditions at the east and west boundaries of the model to allow inflows from the east and outflows to the west. The Mississippi and Missouri Rivers and small ponds were assumed to have a riverbed with a hydraulic conductivity of 9.9 E-5 cm/sec and a thickness of 5 feet. The levels in the rivers fluctuate and affect groundwater flow patterns in the alluvium. Recharge rates were assumed to vary across the SCPA based on inflow and outflow locations as seen in historical aerial photos. General head boundaries were used on the east and west sides of the model in order to allow flow from west to east. These general head boundaries used the calibrated hydraulic conductivities inside the model domain and:

- The western general head boundary: relative head value to the upriver Grafton gauge
- The eastern general head boundary; relative head value to the confluence of the Mississippi and Missouri Rivers.

Groundwater flow was calibrated using a steady state flow model and then checked in a transient analysis. A transient flow model was constructed to complete the transport and closure alternative analyses. To complete this modeling, average annual river levels were calculated for the Mississippi and Missouri rivers from 1987 through 2018 based on available USGS river gauge data. This sequence of 32-years of annually-varying river levels was then applied in future and past years where river conditions are unknown.

### 2.8 Flow Calibration

Flow model calibration was carried out for July 28, 2018 for which 77 groundwater elevations within the alluvial aquifer (at various depths) were available as targets. In addition, 5 pore-water elevations within the SCPA were used from March 9, 2018. This combination was used because there were more targets available in the July 2018 event in the alluvial aquifer and the river levels were more representative of average conditions. Additionally, Pore-water elevations were only collected in February and March of 2018 before the piezometers were abandoned, however, the pond elevation in the SCPA was the same on both March 9, 2018 and July 28, 2018. Therefore, these levels are deemed representative of what pond conditions were in July 2018.

Manual and automated parameter estimation approaches were used to derive reasonable estimates of hydraulic conductivities and natural recharge rates that produce groundwater elevations close to the observed data. The results are summarized in Figure 8. The average head residual is less than 1 feet and the normalized root mean square error in the model is 9.7%. It should be noted that observed groundwater elevations varied from 411.5 – 419.3 feet above mean sea level (ft MSL) in the alluvial aquifer and from 426.5 – 433.4 ft MSL in the SCPA porewater. The calibrated model was found to be acceptable for current purposes.

The calibrated parameters were then used in combination with annually-varying river levels to check the model calibration and provide the basis for flow and transport predictions. Predicted transient groundwater elevations for all of the monitored locations, together with the observed data (black dot), are provided in Appendix A. These data show that the model is also well calibrated under transient flow conditions,

## 2.9 Flow Model Predictions

The calibrated model was used to predict flows from the SCPA, flows rates in the alluvium, flows to/from the river and to optimize recovery well placement and pumping rates for alternate closure scenarios. The scenarios modeled are summarized in Table 2 and Figures 9 to 13.

Future Prediction Model Scenario	Related Figure	Number of Wells	Well Pumping Rate	Total Pumping Rate	Slurry Wall?
Units	NA	NA	(gpm)	(gpm)	NA
SCPA Cap of 1x10 <sup>-7</sup> cm/sec	10				No
SCPA Cap, Hydraulic Containment with Pumping Wells	11	5	3.0	15.0	No
SCPA Cap, Hydraulic Containment with Slurry Wall (100 FT BGS to top of bedrock) and Pumping Wells	12	5	1.0	5.0	Yes
SCPA Cap, Hydraulic Containment with Slurry Wall (150 FT BGS, 50 feet into bedrock) and Pumping Wells	13	5	1.0	5.0	Yes

### Table 2: Summary of Groundwater Flow Model Predictions for Future Scenarios

Notes:

1) cm/sec = centimeters per second

2) FT BGS = feet below ground surface

3) gpm = gallons per minute

4) In all future model scenarios, the SCPA was modeled as drained, inactive, and capped with recharge through the cap to the SCPA of 1-inch per year for a 1.5 feet thick 1 x 10<sup>-7</sup> cm/s soil cover.

5) Hydraulic head control was predicted using proposed pumping wells placed with approximately 500-1000 foot spacing (see reference figures for locations). Each proposed well screen extends from near surface to deep alluvium (layers 1-4).

6) SCPA hydraulic containment was evaluated using predicted flow velocity vectors and predicted pumping well capture of particles distributed along the outside edge and within the southern portions of the SCPA in each model ash layer (see figure 9).

7) The proposed slurry wall was modeled as constructed along the west and south sides of the SCPA from the very shallow alluvium to the top of bedrock (Figure 12) as well as 50 feet into bedrock (Figure 13). The slurry was modeled as 2 feet thick in diameter and a hydraulic conductivity of 1 x 10-6 cm/s.

Groundwater pumping rates are low because:

- The infiltration rate through the capped SCPA is relatively low
- Under capped conditions, the hydraulic gradient is low (nearly flat)
- Under pumping conditions, a hydraulic divide is predicted to develop between the Southern half the SCPA and the Mississippi River to the north, reducing the possibility of pumping river water
- For slurry wall cases, pumping rates are reduced a small amount because the small amount of inflow from the south is reduced
- Additionally, there was no noticeable difference of particles leaving the SCPA between the 100-foot-deep and the 150-foot-deep slurry wall scenarios.

### 2.9.1 Post Closure Flow Around the SCPA

A mass balance analysis was completed to estimate the flow around, verses into the SCPA, after the CCR Unit has equilibrated with the adjacent alluvial aquifer and the recharge into the pond has decreased due to capping and closing the SCPA. This analysis uses the river levels from 1987 through 2018 under capped and closed conditions and takes an average flow from the different hydrostratigraphic units. As shown on Table 3, approximately 87% of groundwater flow is estimated to go around the SCPA and only 13% of groundwater flows into the SCPA. Flow into the SCPA is estimated to be 2.3 gallons per minute on average and flow around the pond is estimated to be 17.5 gallons per minute. The results are illustrated in Figure 14 showing groundwater flow vectors that demonstrate a preferential flow around and under the SCPA rather than into the SCPA.

Table 3:	Model Estimates of Flow Around vs. Into SCPA After Closure	

		Average Flow
	Average Flow (Cubic	(Gallons Per
Average Flow direction	Feet per Day)	Minute)
Flow from NW Alluvial Zone into SCPA	101	0.5
Flow from NE Alluvial Zone into SCPA	122	0.6
Flow from SW Alluvial Zone into SCPA	90	0.5
Flow from SE Alluvial Zone into SCPA	134	0.7
Average Flow from Alluvial Aquifer into SCPA	447	2.3
Flow from SCPA into NW Alluvial Zone	515	2.7
Flow from SCPA into NE Alluvial Zone	507	2.6
Flow from SCPA into SW Alluvial Zone	438	2.3
Flow from SCPA into SE Alluvial Zone 🥄 🛛 🦯	667	3.5
Average Flow from SCPA into Alluvial Aquifer	2126	11
Flow from NW Alluvial Zone into NE Alluvial Zone	826	4.3
Flow from NE Alluvial Zone into NW Alluvial Zone	187	1
Flow from NE Alluvial Zone into SW Alluvial Zone	318	1.6
Flow from SW Alluvial Zone into NE Alluvial Zone	243	1.3
Flow from NE Alluvial Zone into SE Alluvial Zone	430	2.2
Flow from SE Alluvial Zone into NE Alluvial Zone	291	1.5
Flow from SW Alluvial Zone into SE Alluvial Zone	796	4.1
Flow from SE Alluvial Zone into SW Alluvial Zone	278	1.4
Average Total Flow Around the SCPA	3368	17.5
Percent Flow Around vs Through the SCPA	86.9%	

Notes:

- 1) See Figure 14 for information on the different Hydrostratigraphic Units.
- 2) NE Northeast, NW Northwest, SE Southeast, SW Southwest.

### 2.10 Transport Model Analysis

This section describes the transport modeling analyses conducted for the SCPA contaminant source area. The SCPB, SCPC and SCL4A where not modeled as a source area because they are all lined with geomembrane liners while the SCPA is unlined. Based on drilling data and historical images, the SCPA has historically been

managed with the bottom ash contained in the north portions of the CCR unit while and the fly ash has been historically managed in the southern portion of the unit. In 1993, the SCPB was built to the east of the SCPA and fly ash was then managed in the SCPB and not the SCPA.

Molybdenum was selected as the primary constituent for transport analysis because it is the only Appendix IV parameter that is present at a Statistically Significant Level in accordance with the CCR Rule. The primary Molybdenum transport mechanisms are advection and mixing due to natural and pond recharge, advection and mixing under varying natural hydraulic gradients controlled by river water elevations and buffering and/or precipitation due to interaction between Molybdenum in porewater and aquifer solids.

Transport model setup details include:

Aquifer bulk densities based on results from Golder 2018e

- Layer 1:1.7 g/mL
- Layer 2: 1.8 g/mL
- Layers 3 to 6: 1.92 g/mL
- Uniform effective porosity of 0.25
- Longitudinal, transverse and vertical dispersivity were assumed to have values of 1,000, 100, and 10 ft, respectively
- Linear sorption represented by a partition coefficient (Kd) in the aquifer of 1.1 mL/g (Allison and Allison, 2005).
- Molybdenum Concentrations as shown below in Table 4.

#### Table 4: Molybdenum Concentration Data Ranges

Parameter	Reported Range	Model Values	Data Source			
Molybdenum Concentrations (µg/L)						
	Minimum: Non-Detect					
Mississippi River	Maximum: 2.3	1.4	Haley and Aldrich 2018			
	Mean: 1.406		-			
	Minimum: 2.6		Haley and Aldrich 2018			
Missouri River	Maximum: 3.6	3				
	Mean: 2.97					
Background (BMW-1S,	Minimum: Non-Detect					
BMW-3S, BMW-1D, and	Maximum: 9.3	2	Golder 2018 (a-d), Golder 2019 (a-e)			
BMW-3D)	Mean: 1.753					
Bottom Ash (Northern SCPA)	26.5	26.5	Golder 2019b			
Fly Ash / Mixed Ash (Southern SCPA)	1,760 - 56,6000	17,000 (western) 4,000 (central) 2,500 (eastern)	Golder 2019b			

Molybdenum data from November 2018 and January 2018 were included as calibration targets in the model using 73 locations within the alluvial aquifer. During transport model calibration the unknown historical pond levels and concentrations were varied across expected ranges, but the hydraulic parameters were unchanged. The resulting simulated plume, together with the mapped plumes for shallow, intermediate, and deep alluvium are shown in Figures 15-17.

The transport model calibration results are summarized in Figure 18. The average molybdenum concentration residual is less than 30  $\mu$ g/L and the normalized root mean square error is 6.0%. It should be noted that observed molybdenum concentrations varied from Non-detect (1/2 method detection limit at 0.45) – 4,000  $\mu$ g/L in the alluvial aquifer. The calibrated model was found to be acceptable for current purposes.

Predictive simulations were used to assess future plume movement under existing and capped-pond conditions. The predicted future molybdenum concentrations in groundwater were found to be sensitive to the assumed partition coefficient and the infiltration rate through the cap. SCPA ash pore-water concentrations after capping and closure were simulated in two different ways:

- With a concentration that remained constant prior to and after closing the SCPA
- With a concentration that was reduced to zero directly after closing the SCPA

Reality is likely to fall somewhere between these two cases. In both of these scenarios, the recharge through the cap was assumed to be reduced to 1 inch/year (0.000229 feet per day). After capping the heads in the pond and flow out of the base of the pond are predicted to gradually decrease over time. Predicted concentrations for groundwater concentrations in the alluvium for these two scenarios are provided in Figures 19, 20, and 21. These figures show that in monitoring wells directly adjacent to the pond, molybdenum concentrations can range about 10-20% in concentration depending on the attenuation of the residual molybdenum left in the SCPA after closure. Model predicted plume maps looking at the first scenario (constant concentration) are provided in Appendix B and represent a worst-case scenario for residual molybdenum concentrations.

Model estimated concentrations in the plume were predicted to:

- Continue to slowly increase in extent at the edge (corresponding to historical migration from the uncapped pond)
- Slowly decrease in the aquifer beneath and close to the pond as molybdenum flux from the pond decreases.
  Adjacent to the pond, molybdenum concentrations are estimated to decrease about 75% over 200 years.
- Continue to have molybdenum concentrations that are greater than the site Ground Water Protection Standard (GWPS) within the property boundary to the west, south, and east of the SCPA.
- Pumping effects on the future molybdenum plume were not evaluated.
- model assumes the median Kd value from Allison (2005) for this site. If site specific soil testing were completed and a lower Kd value was determined, molybdenum concentrations would decline at a faster rate after closure.

## 3.0 GEOCHEMICAL ASSESSMENT

### 3.1 Overview

Groundwater was evaluated to determine the feasibility of Monitored Natural Attenuation (MNA) as part of the Assessment of Corrective Measures (ACM) for the SEC. The structure of this feasibility evaluation closely follows the USEPA guidance on using MNA as a remedial strategy (USEPA 2007a and 2007b) and considers best practices from the Interstate Technology Regulatory Council (ITRC) document: "A Decision Framework for Applying Monitored Natural Attenuation Processes to Metals and Radionuclides in Groundwater" (ITRC 2010).

## 3.2 Approach

To assess the geochemical feasibility of MNA at the ACM screening level, laboratory analyses of groundwater collected in November 2018 for samples in the alluvial aquifer and in January 2018 for pore-water samples collected in the SCPA and SCPB. This data provided a comprehensive geochemical dataset. Historical molybdenum concentrations in groundwater from March 2016 to November 2018 was used for plume stability evaluation (Golder 2018a, 2018b, 2018c, 2018d, 2019a, 2019b, 2019c, and 2019d). Monitoring wells and piezometers selected for this evaluation included CCR rule (monitoring) wells for the SCPA and SCPB, nature and extent monitoring wells, and pore-water piezometers from inside the ash impoundment (Table 5). Parameters (description of laboratory methods is included in the above references) included in the geochemical assessment included field parameters (pH, dissolved oxygen, oxidation reduction potential (ORP), conductivity, and temperature), Appendix III and IV parameters, and major Cations and Anions.

#### Table 5: Monitoring Wells and Piezometers Included in the Geochemical Assessment

CCR Rule Wells	Nature and Extent Wells	Pore-water Piezometers
SCPA -S-UMW-1D, S-UMW-2D, S-UMW-	S-TP-1D, S-TP-1S-TP-1S, S-TP-2D, S-TP-	S-SCPA-2, S-SCPA-3S,
3D, S-UMW-4D, S-UMW-5D, S-UMW-6D,	2M, S-TP-2S, S-TP-3D, S-TP-3M, S-TP-	S-SCPA-1D, S-SCPA-3D
SCPB -S-LMW-1S, S-LMW-2S, S-LMW-3S,	3S, S-TP-4D, S-TP-4M, S-TP-4S, S-TP-5D,	
S-LMW-4S, S-LMW-5S, S-LMW-6S, S-	S-TP-5M, S-TP-5S, S-TP-6D, S-TP-6M, S-	
LMW-7S, S-LMW-8S, S-LMW-9S,	TP-6S, S-TP-7D, S-TP-7M, S-TP-7S, S-TP-	
Background -S-BMW-1D(bg),S-BMW-	8D, S-TP-8M, S-TP-8S, AM-1S (UMW-7S),	
3D(bg), S-BMW-1S(bg), S-BMW-3S(bg)	AM-1D (UMW-7D)	

Note: (bg) indicates background CCR rule monitoring well

The geochemical assessment of groundwater from the above identified locations included:

- Groundwater characterization to identify temporal and geographical trends, where present
- Geochemical modeling to identify the major chemical species and evaluation of saturation indices of minerals relevant to attenuation of molybdenum

Based on the results generated of this assessment, a screening-level attenuation evaluation was completed to determine the potential geochemical controls on molybdenum.

### 3.2.1 Geochemical Modeling

Geochemical modeling was conducted to evaluate general groundwater and pore-water quality, determine the potential for precipitation of sorbent media, evaluate the potential for mineral precipitation or adsorption in the

aquifer, and determine the speciation of metals of interest. The geochemical computer code developed by the United States Geological Survey (USGS), PHREEQC, was used for these simulations (Parkhurst and Appelo 2013). PHREEQC version 3.4 is a general-purpose geochemical modeling code developed by the USGS and used to simulate reactions in water and between water and solid mineral phases (e.g., rocks and sediments). Reactions include aqueous equilibria, mineral dissolution and precipitation, ion exchange, surface complexation, solid solutions, gas-water equilibrium, and kinetic biogeochemical reactions. The widely-accepted thermodynamic database, Minteq.v4, 2017 edition, was used as a basis for the thermodynamic constants required for modeling.

The Geochemist's Workbench version 12 (Bethke 2015) was used to generate graphical representations of geochemical modeling outputs in the form of predominance, or Pourbaix diagrams (also known as Eh-pH diagrams) for the species of interest (i.e. cobalt, lithium, and molybdenum) and trilinear plots (also known as Piper plots) of the relative abundance of major ions. The Minteq.v4 database was also used as the basis for the Pourbaix diagrams.

The potential for mineral precipitation was assessed in PHREEQC using a saturation index (SI) calculated according to Equation 1.

(Equation 1)

The saturation index is the ratio of the ion activity product (IAP) of a mineral to the solubility product (Ksp). An SI value greater than zero indicates that the water is supersaturated with respect to a particular mineral phase and, therefore, precipitation of the mineral may occur. An evaluation of precipitation kinetics is then required to determine whether the supersaturated mineral will indeed form. An SI value less than zero indicates the water is undersaturated with respect to a particular mineral phase. An SI value close to zero indicates equilibrium conditions exist between the mineral and the solution. SI values between -0.5 and 0.5 are referred to as 'at equilibrium' in this report.

### 3.2.2 Assumptions and Data Handling

Geochemical modeling assumptions and data handling included:

- Groundwater continuity: Groundwater quality data from a single sampling event conducted in November 2018 were evaluated. This sampling event was selected because the most wells were sampled and analyzed for the full suite of parameters. Temporal trend analysis for molybdenum, made use of available sampling events.
- Pore-water chemistry: Pore-water data was assumed to be representative of porewater found in ash impoundment based on the four porewater piezometer samples.
- Redox values: ORP values measured in the field were converted to reduction potential (Eh) by adding 200 millivolts (mV) to the field-measured values as per YSI (2015).
- **Non-detect values:** Constituents with concentrations not detected above the method detection limit were assumed to have a concentration equal to half the reporting limit in model simulations.
- **Charge balance:** Groundwater compositions with charge balance errors less than 10% were considered valid. Compositions with charge balance errors greater than 10% were not considered in the evaluation.

### 3.3 Groundwater characterization

Water quality monitoring data is summarized as follows:

- Charge balance error: There was one groundwater sample from November 2018 with a charge balance error of greater than 10% (S-UMW-3D). These results were retained and used during this evaluation, with the understanding that they may be somewhat less reliable.
- **pH:** Groundwater pH across the well network ranged from 6.1 to 8.9. The geometric mean pH across all wells was 7.0. Highest pH was measured in porewater at 8.9. The nature and extent wells ranged from 6.1 to 7.3.
- ORP (Redox): Field-measured redox, corrected to Eh (+200mV) values, ranged from +8 to +410 mV across the site. There was no apparent trend in redox conditions based on sample location or depth.
- Total Dissolved Solids (TDS): Groundwater TDS concentrations were variable. The lowest TDS concentrations (300 to 400 mg/L) occurred in groundwater in CCR rules wells, both in downgradient and background wells. The highest TDS concentration (2,200 to 2,900 mg/L) was measured in the porewater, shallow and deep wells of S-SPCA-3 (S/D). In general, all other wells (including pore-water in SPCA-1 and 2 wells) had TDS less than half of that measured in SPCA-3S/D.
- Major ion chemistry: A Piper plot was generated for all background, monitoring, and assessment wells to facilitate the identification of water types and changes in major ion chemistry over time (Figure 22a and 22b). In general, most of the shallow SCPB (LMW) and deeper SCPA (UMW) CCR groundwater monitoring wells can be identified to be a mix of background and pore-water from S-SCPA-1/2 (Figure 22a). S-UMW-2D and 3D show the most similarity to the porewater in SCPA-3S/D. However, nature and extent wells (Figure 22b) indicate they have dissimilar overall groundwater major ion chemistry than that of S-SPCA-3S/D.
- Molybdenum: Molybdenum concentrations in groundwater at monitoring wells (CCR rule and nature and extent) ranged from non-detect (<0.0005 mg/L) to 4.0 mg/L in November 2018. Six groundwater samples from CCR rule wells contained molybdenum greater than 100 µg/L (S-UMW-2D, 3D, 4D, 5D, and S-LMW-2S, 5S), the health-based standard. The molybdenum concentration in porewater has ranged from 0.03 to 56.6 mg/L (SPCA-1S; not included in geochemical modeling). Although the highest molybdenum in CCR rules wells exceeded the health-based standard, levels of molybdenum were an order of magnitude lower than the highest measured in porewater. Only two nature and extent wells exceeded the health-based standard (S-AM-1D (UMW-7D) and S-TP-5D). However, as shown in Figure 1, S-TP-5D is not located at the property boundary and AM-1D is located within 150 feet of the SCPA. The level of molybdenum in groundwater in CCR rule wells since March 2016 to November 2018 shows a general stable or downward trend since 2016 in all CCR Rule wells around the SCPA and SCPB, indicating a stable or decreasing plume (Figure 23a-c). Molybdenum is predominately present in the form of the divalent anion species molybdate (MoO4<sup>-2</sup>) based on field measured pH and redox conditions (Figure 22c).
- Iron: Total (un-filtered) iron concentrations were variable, ranging from non-detect (<0.012 mg/L) to 22 mg/L in November 2018. The highest concentration of 22 mg/L was detected in the groundwater sample collected from nature and extent well S-TP-1S. No geographical or depth trend is apparent; however, nature and extent wells generally tended to have higher total iron contents as a group. Ferric iron concentrations were higher than ferrous iron concentrations in all samples collected in November 2018.</p>

In summary, the results of the groundwater quality evaluation indicate there are no initial indications or geochemical conditions that would be detrimental to attenuation of molybdenum at the Ameren SEC site. In addition, the positive redox across all wells at the site and the dominance of ferric iron over ferrous iron in groundwater are favorable indicators for the potential success of MNA.

## 3.4 Geochemical Modeling Results

The results of speciation modeling of groundwater at background, downgradient, and nature and extent wells are provided in Appendix C, including saturation indices for relevant minerals. Mineral saturation is important to identify when considering solid phases that may influence attenuation of metals, directly through precipitation, or indirectly by providing a sportive surface for metals to be removed from groundwater.

- Iron-bearing minerals: Ferrihydrite (Fe(OH)<sub>3</sub>) was indicated to be at equilibrium with groundwater or oversaturated in all samples, indicating a strong potential for ongoing precipitation of solid phase iron oxides. Thus, throughout the Ameren SEC site, the prevalence of iron oxides is assumed.
- Other minerals: Nearly all groundwater samples were in equilibrium with respect to rhodochrosite (MnCO<sub>3</sub>). Manganese presents an additional potential adsorption surface for attenuation. Calcite (CaCO<sub>3</sub>) equilibrium was indicated in numerous wells as well. Calcite can provide a mechanism to maintain groundwater pH. Barite (BaSO<sub>4</sub>) equilibrium was also indicated in numerous wells, and Gypsum (CaSO<sub>4</sub>:2H<sub>2</sub>O) equilibrium was present in two piezometers (S-SCPA-3S/D).

In summary, several mineral phases likely control groundwater composition at some or all wells: barite, calcite, ferrihydrite, gypsum, and rhodochrosite. In the case of ferrihydrite and rhodochrosite, the dissolved concentrations of constituents can be reduced through its ability to act as a substrate for adsorption (Dzombak and Morel 1990).

## 4.0 CONCLUSIONS

Based on both the groundwater flow model, the transport simulations and a geochemical analysis described in this report, the following conclusions can be made:

- Groundwater concentrations for Molybdenum are modeled to be slow moving, and concentrations above the GWPS stay within Ameren property boundaries to the west, south and east and in the leased area to the north.
- Molybdenum concentrations decrease by more than 75% in the 200-year post closure model estimation for monitoring wells with the highest current molybdenum concentrations.
- Based on data collected since 2016, the stable or decreasing trend in molybdenum concentrations in all CCR rule wells and lack of molybdenum above the health-based standard in monitoring wells on the western, southern and eastern portions of the property boundary indicate that plume from the ash impoundments are stable. The results of the groundwater quality evaluation indicate there are no indications or geochemical conditions that would be detrimental to natural attenuation of molybdenum at the Ameren SEC site.
- Based on geochemical modeling results, coupled with the site size, the apparent plume stability, and lack of molybdenum above the GWPS in all but one monitoring well to the north, attenuation of molybdenum is likely occurring, meeting the requirements of this initial modeling effort and MNA assessment.

## 5.0 LIMITATIONS

The modeling analyses presented in this report are a simplification of reality and the model-predicted results should be used with this understanding. The limitations associated with analyses such as these are detailed below.

Hydrogeologic investigations and groundwater modeling are dynamic and inexact sciences. They are dynamic in the sense that the state of any hydrological system is changing with time, and in the sense that the science is continually developing new techniques to evaluate these systems. They are inexact in the sense that groundwater systems are complicated beyond human capability to evaluate them comprehensively in detail, and we invariably do not have sufficient data to do so. A groundwater model uses the laws of science and mathematics to draw together the available data into a mathematical or computer-based representation of the essential features of an existing hydrogeologic system. While the model itself obviously lacks the detailed reality of the existing hydrogeologic system, the behavior of a valid groundwater model reasonably approximates that of the real system. The validity and accuracy of the model depends on the amount of data available relative to the degree of complexity of the geologic formations, the site geochemistry, the fate and transport of the dissolved compounds, and on the quality and degree of accuracy of the data entered. Therefore, every groundwater model is a simplification of a reality and the model described in this report is not an exception.

The professional groundwater and geochemical modeling services performed as described in this report were conducted in a manner consistent with that level of care and skill normally exercised by other members of the engineering and science professions currently practicing under similar conditions, subject to the quality and quality of available data, the time limits and financial and physical constraints applicable to the services. Unless otherwise specified, the results of previous or simultaneous work provided by sources other than Golder and quoted and/or used herein are considered as having been obtained according to recognized and accepted professional rules and practices, and therefore deemed valid. This model provides a predictive scientific tool to evaluate the impacts on a real groundwater system of specified hydrological stresses and/or to compare various scenarios in a decision-making process. However, and despite the professional care taken during the construction of the model and in conducting the simulations, its accuracy is bound to the normal uncertainty associated to groundwater modeling and no warranty, express or implied, is made.

### Tables:

- Table 1 Model Input Data Ranges
- Table 2 Summary of Groundwater Flow Model Predictions for Future Scenarios
- Table 3 Model Estimates of Flow Around vs Into SCPA After Closure
- Table 4 Molybdenum Concentration Data Ranges
- Table 5 Monitoring Wells and Piezometers Included in the Geochemical Assessment

#### Figures:

- Figure 1 Sampling Location Map
- Figure 2 Groundwater Model Domain
- Figure 3 Groundwater Model Grid and Cross Section Location Map
- Figure 4 A-A' Cross-Section and Hydraulic Conductivities
- Figure 5 B-B' Cross Section and Hydraulic Conductivities
- Figure 6 Recharge Distribution
- Figure 7 Other Model Boundary Conditions
- Figure 8 Scatter Diagram for Predicted and Observed Hydraulic Heads
- Figure 9 Transient Groundwater Model Starting Particle Locations for Forward Particle Tracking

Figure 10 – Transient Groundwater Model Predictions – Historical (No Cap) and Future (With Cap) Conditions with Forward Particle Flow Paths

Figure 11 – Transient Groundwater Model Predictions with Closed (1x10<sup>^</sup>-7 cm/sec cap) SCPA With Five Proposed Pumping Wells

Figure 12 – Transient Groundwater Model Predictions with Closed (1x10<sup>^</sup>-7 cm/sec Cap) SCPA, Slurry Wall (100 FT BGS), and Five Proposed Pumping Wells

Figure 13 – Transient Groundwater Model Predictions with Closed (1x10<sup>-7</sup> cm/sec Cap) SCPA, Slurry Wall (100 FT BGS), and Five Proposed Pumping Wells

Figure 14 – Model Estimates of Flow Around vs Into the SCPA Figure 15 – Predicted and Observed Molybdenum Concentrations – Shallow Alluvial Aquifer

Figure 15 - Predicted and Observed Molybdenum Concentrations – Shallow Alluvial Aquifer

- Figure 16 Predicted and Observed Molybdenum Concentrations Intermediate Alluvial Aquifer
- Figure 17- Predicted and Observed Molybdenum Concentrations Deep Alluvial Aquifer
- Figure 18 Scatter Diagram for Predicted and Observed Molybdenum Concentrations

Figure 19 – Predicted Molybdenum Concentrations at UMW-2D for Alternate Assumed Post Closure SCPA Porewater Concentrations

Figure 20 – Predicted Molybdenum Concentrations at UMW-3D for Alternate Assumed Post Closure SCPA Porewater Concentrations

Figure 21 – Predicted Molybdenum Concentrations at UMW-4D for Alternate Assumed Post Closure SCPA Porewater Concentrations

Figure 22 – Major Ion Geochemistry



Figure 23 – Molybdenum Trends

#### Appendices:

- Appendix A Model Predicted and Observed Transient Groundwater Level Elevations
- Appendix B Molybdenum Concentration Time Histories for Intermediate Alluvial Aquifer
- Appendix C Speciation Modeling

### 6.0 REFERENCES

- Allison, J.D. and T.L. Allison (2005). Partition Coefficients for Metals in Surface Water, Soil, and Waste. EPA/600/R-05/074
- Ameren 2017, State of Missouri Department of Natural Resources Missouri Clean Water Commission Missouri State Operating Permit M0-0000353. National Pollutant Discharge Elimination System (NPDES)
- Bethke, C., 2015. Geochemist's Workbench: Release 12.0 Aqueous Solutions, LLC.
- Dzombak, D.A. and Morel, F., 1990. Surface complexation modeling: hydrous ferric oxide. John Wiley & Sons.
- Environmental Simulations Inc. (ESI), 2016. Groundwater Vistas version 6.85 Build 16.
- Electric Power Research Institute (EPRI). 1998, Field Evaluation of the Comanagement of Utility Low-Volume Wastes with High-Volume Coal Combustion By-Products: SX Site. September 1998.
- Fetter, C.W. 2000. Applied Hydrogeology, Fourth Edition. Pearson Education. Haley and Aldrich 2018. HELP Model results for different cap scenarios.
- GREDELL Engineering Resources, Inc. 2006. Detailed Geologic and Hydrologic Site Investigation Report. AmerenUE Sioux Power Plant Proposed Utility Waste Disposal Area. St. Charles County, Missouri. August 2006.
- GREDELL Engineering Resources, Inc. 2009. Background Groundwater Monitoring Report. AmerenUE Sioux Power Plant. St. Charles County, Missouri. June 2009.
- Golder Associates Inc., 2017a, 40 CFR Part 257 Groundwater Monitoring Plan, SCPA Sioux Energy Center St. Charles County, Missouri, USA.
- Golder Associates Inc., 2017b, 40 CFR Part 257 Groundwater Monitoring Plan, SCPB Sioux Energy Center St. Charles County, Missouri, USA.
- Golder Associates Inc., 2017c, 40 CFR Part 257 Groundwater Monitoring Plan, SCPC Sioux Energy Center St. Charles County, Missouri, USA.
- Golder Associates Inc., 2017d, 40 CFR Part 257 Groundwater Monitoring Plan, SCL4A Sioux Energy Center St. Charles County, Missouri, USA.
- Golder Associates Inc., 2018a, 2017 Annual Groundwater Monitoring Report, SCPA Bottom Ash Surface Impoundment, Sioux Energy Center St. Charles County, Missouri, USA.

- Golder Associates Inc., 2018b, 2017 Annual Groundwater Monitoring Report, SCPB Fly Ash Surface Impoundment, Sioux Energy Center St. Charles County, Missouri, USA.
- Golder Associates Inc., 2018c, 2017 Annual Groundwater Monitoring Report, SCPC Utility Waste Landfill Surface Impoundment, Sioux Energy Center St. Charles County, Missouri, USA.
- Golder Associates Inc., 2018d, 2017 Annual Groundwater Monitoring Report, SCL4A Utility Waste Landfill Cell 4A, Sioux Energy Center St. Charles County, Missouri, USA.
- Golder Associates Inc., 2018e, SCPA Pond Closure Design Report, Sioux Energy Center (SEC).
- Golder Associates Inc., 2019a, 2018 Annual Groundwater Monitoring and Corrective Action Report, SCPA Surface Impoundment, Sioux Energy Center, St. Charles County, Missouri, USA.
- Golder Associates Inc., 2019b, 2018 Annual Groundwater Monitoring and Corrective Action Report, SCPB Surface Impoundment, Sioux Energy Center, St. Charles County, Missouri, USA.
- Golder Associates Inc., 2019c, 2018 Annual Groundwater Monitoring and Corrective Action Report, SCPC Surface Impoundment, Sioux Energy Center, St. Charles County, Missouri, USA.
- Golder Associates Inc., 2019d, 2018 Annual Groundwater Monitoring and Corrective Action Report, SCL4A Utility Waste Landfill Cell 4A, Sioux Energy Center, St. Charles County, Missouri, USA.
- Golder Associates Inc., 2019e, Nature and Extent Investigation, Sioux Energy Center, St. Charles County, Missouri, USA.
- Haley and Aldrich 2018, Human Health and Ecological Assessment of the Sioux Energy Center. Ameren Missouri, St. Louis, Missouri.
- Harbaugh, Arlen W., 2005, MODFLOW-2005; The U.S. Geological Survey Modular Ground-water Model-The Ground-water Flow Process. (U.S. Geological Survey Techniques and Methods 6-A16).
- Harbaugh, Arlen W., E.R. Banta, M.C. Hill, and M.G. McDonald, 2000. MODFLOW-2000; The U.S. Geological Survey Modular Ground-water Model—User Guide to Modularization Concepts and the Ground-water Flow Process. (Open File Report 00-92). U.S. Geological Survey, 121 p.
- Harbaugh, Arlen W. and M.G. McDonald, 1996. User's Documentation for MODFLOW-96, An Update to the U.S. Geological Survey Modular Finite-Difference Ground-water Flow Model. (Open File Report 96- 485). U.S. Geological Survey, 56 p.
- ITRC, 2010. A Decision Framework for Applying Monitored Natural Attenuation Processes to Metals and Radionuclides in Groundwater. Technical/Regulatory Guidance.
- Morris, D.A. and A.I. Johnson, 1967. Summary of hydrologic and physical properties of rock and soil materials as analyzed by the Hydrologic Laboratory of the U.S. Geological Survey, U.S. Geological Survey Water-Supply Paper 1839-D, 42p.
- McDonald, M. G., and A. W. Harbaugh, 1988. A Modular Three-dimensional Finite-Difference Groundwater Flow Model. (Techniques of Water-Resources).
- Owuor et al., 2016. Groundwater Recharge Rates and Surface Water Runoff Response to Land Use and Land Cover Changes in Semi-Arid Enviroments.

- Parkhurst, D.L. and Appelo, C.A.J., 2013. Description of input and examples for PHREEQC version 3: a computer program for speciation, batch-reaction, one-dimensional transport, and inverse geochemical calculations (No. 6-A43). US Geological Survey.
- Pollock, D.W., 2012. User Guide for MODPATH Version 6 A Particle-Tracking Model for MODFLOW: U.S. Geological Survey Techniques and Methods 6–A41, 58 p.
- Rietz & Jens, Inc., and GREDELL Engineering Resources, Inc. 2014. Ameren Missouri Sioux Power Plant Utility Waste Landfill – Proposed Construction Permit Modification – Construction Permit Number 0918301 – St. Charles County, Missouri, revised August 2014.
- Rumbaugh, J.O., and Rumbaugh, D.B., 2011. Guide to Using Groundwater Vistas Version 6. Environmental Simulations, Inc., Reinholds, Pennsylvania
- Smith, K.S. and Huyck, H.L., 1999. An overview of the abundance, relative mobility, bioavailability, and human toxicity of metals. The environmental geochemistry of mineral deposits, 6, pp.29-70.
- State of Missouri Department of Natural Resources Missouri Clean Water Commission, 2017. Missouri State Operating Permit Permit No. MO-0000353.
- USGS 2019. National Water Information System USGS gauges 05587498, 05587450, 06935965, and 07010000.
- USGS 2010. Groundwater-Flow Assessment of the Mississippi River Valley Alluvial Aquifer of Northeastern Arkansas. Scientific Investigations Report 2010-5210.
- USGS 2001. Hydrogeology, Model Description, and Flow Analysis of the Mississippi River Alluvial Aquifer in Northwestern Mississippi. Water-Resource Investigations Report 2001-4035.
- YSI. 2015. Tech Note, Measuring ORP on YSI 6-Series Sondes: Tips, Cautions and Limitations.
- Zheng, Chunmiao, and P. Patrick Wang, 1999, MT3DMS, A modular three-dimensional multi-species transport model for simulation of advection, dispersion and chemical reactions of contaminants in groundwater systems; documentation and useri s guide, U.S. Army Engineer Research and Development Center Contract Report SERDP-99-1, Vicksburg,



Figures









4 N	<b>JFR</b>	FN	00004031	



			Kx,	, Ку	k	ζz
	Color	Layer 🍋	cm/sec	ft/day	cm/sec	ft/day
		Top Stratum (Silts/Clays)	9.9E-04	2.8	9.9E-04	2.8
		Shallow Alluvium (Sands and Silts)	2.6E-02	75	2.6E-03	7.5
		Intermediate Alluvium (Sands)	4.0E-02	113	4.0E-03	11.3
		Deep Alluvium (Sands and Gravels)	5.3E-02	150	5.3E-03	15
		SCPA - Fly Ash	1.8E-04	0.5	1.8E-05	0.05
		SCPA - Bottom Ash	1.8E-04	0.5	1.8E-05	0.05
		Embankments	2.7E-06	0.008	9.9E-09	2.80E-05
		Plant Areas (High Ground)	8.0E-04	2.3	8.1E-04	2.3
		Lined CCR Units	3.0E-03	8.5	3.0E-04	0.85
		Bedrock	9.9E-07	0.0028	9.9E-08	0.00028
		Surface Water		NLA		
		No Flow		NA	NA NA	NA
ertical e second	exaggeration. I.	CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER	Ame	PROJEC GROU	NDWATER MON	TORING PROGRAM
ion loc	ation.	CONSULTANT YYYY-MM-DD	2019-03-07	TITLE A-A' (	Cross-Section a	nd Hydraulic Conduc
		PREPARED	JSI			•

NOTE(S)

- 1) Cross-section has a 10X ve
- 2) Cm/sec = centimeters per s
- 3) Ft/day = feet per day.
- 4) See Figure 3 for cross section



DESIGN REVIEW APPROVED JSI

153-1406

JM

MNH

TITLE A-A' Cross-Section and Hydraulic Conductivities					
PROJECT No. 153-1406	REV. <b>0.0</b>	FIGURE			

4



# 15X Vertical Exaggeration

		Kx,	, Ку	K	ζz
Color	Layer	cm/sec	ft/day	cm/sec	ft/day
	Top Stratum (Silts/Clays)	9.9E-04	2.8	9.9E-04	2.3
	Shallow Alluvium (Sands and Silts)	2.6E-02	75	2.6E-03	7.
	Intermediate Alluvium (Sands)	4.0E-02	113	4.0E-03	11.
	Deep Alluvium (Sands and Gravels)	5.3E-02	150	5.3E-03	1
	SCPA - Fly Ash	1.8E-04	0.5	1.8E-05	0.0
	SCPA - Bottom Ash	1.8E-04	0.5	1.8E-05	0.0
	Embankments	2.7E-06	0.008	9.9E-09	2.80E-0
	Plant Areas (High Ground)	8.0E-04	2.3	8.1E-04	2.
	Lined CCR Units	3.0E-03	8.5	3.0E-04	0.8
	Bedrock	9.9E-07	0.0028	9.9E-08	0.0002
	Surface Water	NLA	NLA	NLA	
	No Flow	NA	NA	NA	NA

YYYY-MM-DD

PREPARED

DESIGN

REVIEW

APPROVED

NOTE(S)

- Cross-section has a 15X vertic 1)
- 2) Cm/sec = centimeters per second.
- 3) Ft/day = feet per day.
- See Figure 3 for cross section location. 4)



GOLDER



2019-03-07

JSI

JSI

JM

MNH

RAM

PROJECT No.

153-1406

B-B' Cross-Section and Hydraulic Conductivities

REV.	FIGUR
0.0	Ę



Color	Layer	Feet p	er day	Inches	per year
	Wooded Areas	0.00	059		2.6
	Built up Plant Areas	0.00	059		2.6
	Agricutural Areas	0.00	059		2.6
	Surface Water/ Line CCR Units	N	A		NA
	No Flow	NA		NA	
SCPA Conditions (Transient Conditons)					
		Active	Capped	Active	Capped
	Western Bottom Ash SCPA	0.015		66	
	Central Bottom Ash SCPA	0.02		88	
	Eastern Bottom Ash SCPA	0.03	0.00023	131	1.0
	Eastern Fly Ash SCPA	0.025		110	
	Central Fly As SCPA	0.02		88	
	Western Fly Ash SCPA	0.015		66	

#### CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER

🕓 GOLD

CONSULTANT



PROJECT GROUNDWATER MODELING

#### TITLE RECHARGE DISTRIBUTION

Project 153-1406

		MNH
	REVIEW	IM
ER	DESIGN	JSI
	PREPARED	JSI

### AMEREN\_00004034

Rev. 0.0 FIGURE

CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER  Image: Consultant  YYYY-MM-DD  2018-03-07    CONSULTANT  YYYY-MM-DD  2018-03-07  TITLE    PREPARED  JSI  DESIGN  JSI    REVIEW  JM  Project  Rev.		a) - GHB is placed of a represent surface		Partial States    Compare the same same same same same same same sam	obe @CNES (20	rater features.
CONSULTANT    YYYY-MM-DD    2018-03-07    TITLE      PREPARED    JSI    DESIGN    JSI      REVIEW    JM    Project    Rev.      FIGURE    FIGURE    FIGURE	CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER		<b>Mameren</b>	PROJECT GROUNDWATER MODELING		, the thickness of the
163.1/06 0.0 7.1	GOLDER	YYYY-MM-DD PREPARED DESIGN REVIEW	2018-03-07 JSI JSI JM	TITLE OTHER MODEL BOUNDARY CONDITION	Rev.	FIGURE









#### Particle Trace Colors

 SCPA or Top Stratum (Layer 1)		
 SCPA or Shallow Alluvium (Layer 2)		
 Intermediate Alluvium (Layer 3)		
 Deep Alluvium (Layer 4)		

#### Model Boundary Condition Cells

River



CONSULTANT

CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER



-5 Proposed Pumping Wells at approximately 500 to 1000 foot

spacing -Screened from Very Shallow Alluvium to Deep Alluvium (Layers 1-4) -Upward Vertical Hydraulic Gradient predicted in Deep Alluvium near each well

-Predicted hydraulic containment of southern SCPA particles maintained based on:

-Each Well Pumping Rate = **3 gpm** Total Pumping Rate = **15 gpm** 

1531406

NOTE(S) - Transient groundwater model predictions. - Particles distributed along the outside edge of the SCPA in each model ash layer. See Figure 9 for details on starting particle locations. - Cap model includes 1.0 inches/year recharge to the SCPA based model net infiltration prediction for 1 x 10<sup>4</sup>-7 cm/s soil cover.



GROUNDWATER MONITORING PROGRAM



#### TRANSIENT GROUNDWATER MODEL PREDICTIONS WITH CLOSED (1x10^-7 CAP CM/SEC CAP) SCPA WITH FIVE PROPOSED PUMPING WELLS PROJECT NO. REV. FIGURE

11

Α



Α

12



A	
AMERE	N_00004041

13












S









Maior	lon	Geor	hom	ictr

TITLE			

GROUNDWATER MONITORING PROGRAM

TITLE	
-------	--

PROJECT

## Major Ion Geochemistry

			F
PROJECT NO.	PHASE	REV.	FIGURE
1531406	0003		22 F

	S-TP-1D
	S-TP-1M
	S-TP-1S
	S-TP-2D
•	S-TP-2M
0	S-TP-2S
	S-TP-3D
4	S-TP-3M
4	S-TP-3S
	S-TP-4D
7	S-TP-4M
V	S-TP-4S
	S-TP-5D
۰	S-TP-5M
٠	S-TP-5S
1	S-TP-6D
· X	S-TP-6M
XX	S-TP-6S
ें। ★	S-TP-7D
0 📩	S-TP-7M
1	S-TP-7S
$\overline{\mathbf{x}}$	S-TP-8D
23	S-TP-8M
	S-TP-8S
0	S-SCPA-1D
0	S-SCPA-2
	S-SCPA-3S
X	S-SCPA-3D





APPENDIX A

Model Predicted and Observed Transient Groundwater Level Elevations

Page 1 of 5









Page3 of 5

Page4 of5



Page5 of5



APPENDIX B

## Molybdenum Concentration Time Histories for Intermediate Alluvial Aquifer















	SC	PA			Time Year	Step: 61 2028
	2000 2000 200					
bing			© 2019 Microsof Distribution Airbu	t Corporation © 2019 I Is DS	DigitalGlobe ©CNE	S (2019)
LEGEND	oundary		NOTES 1. PLUME CONC	CENTRATIONS CALCUL	ATED USING GROUN	NDWATER VISTAS,
SCPA - Unlined Bottom Ash Sur	face Impoundmen	t	MODFLOW, AND 2. PLUME REPI	DIMIBUS. RESENTS CONCENTRA FLEVATION OF APPROX	TIONS IN LAYER 3 C	F THE MODEL AT
Molybdenum Concentrations Green	eater Than 100 (µ	g/L)		1 000	2 000	3 000
Molybdenum Concentrations Gr	eater Than 1000 (	μg/L)		1,000	_,000	
CLIENT AMEREN MISSOURI SIQUX ENERGY CENTER	eater Than 3000 (	<sup>µg/L)</sup>	PROJECT GROUNDWAT	ER MODELING		
	YYYY-MM-DD PREPARED DESIGN	2019-03-12 EFT	TITLE MODEL PRED YEAR 61 (202	DICTED MOLYBDEN 8) - CAPPED AND C	UM CONCENTRA LOSED SCPA	TION MAP
<b>*</b>	REVIEW	JSI MNH	Project 153-1406		Rev. 0.0	FIGURE

NUT	Time Step: 71         Year: 2038
LEGEND         Sioux Energy Center Property Boundary         SCPA - Unlined Bottom Ash Surface Impoundment         Molybdenum Concentrations Greater Than 100 (µg/L)         Molybdenum Concentrations Greater Than 1000 (µg/L)         Molybdenum Concentrations Greater Than 3000 (µg/L)         CLIENT         MAREREN MISSOURI SIOUX ENERGY CENTER         CONSULTANT         YYYY-MM-DD       2019-03-12         PREPARED         ESIGN       JSI         REVIEW       JSI         REVIEW       JSI         APPROVED       MNH	O 2019 Microsoft Corporation © 2019 DigitalGlobe ©CNES (2019) Distribution Airbus DS

	Time Step: 81 Year: 2048
LEGEND         Sinux Energy Center Property Boundary         Sinux Energy Center Property Boundary         Sinux Energy Center Property Boundary         Molybdenum Concentrations Greater Than 100 (µg/L)         Molybdenum Concentrations Greater Than 1000 (µg/L)         Molybdenum Concentrations Greater Than 1000 (µg/L)         Molybdenum Concentrations Greater Than 1000 (µg/L)         Molybdenum Concentrations Greater Than 3000 (µg/L)         CUNT	Other sector   Other sector
GOLDER     PREPARED     EFT       DESIGN     JSI       REVIEW     JSI       APPROVED     MNH	Project     Rev.     FIGURE       153-1406     0.0     A9

SCPA	Time Step: 91         Year: 2058
	<image/>
bing	© 2019 Microsoft Corporation © 2019 DigitalGlobe @CNES (2019)
LEGEND Sioux Energy Center Property Boundary SCPA - Unlined Bottom Ash Surface Impoundment Molybdenum Concentrations Greater Than 100 (µg/L) Molybdenum Concentrations Greater Than 1000 (µg/L) Molybdenum Concentrations Greater Than 3000 (µg/L)	NOTES         1. PLUME CONCENTRATIONS CALCULATED USING GROUNDWATER VISTAS, MODFLOW, AND MT3DS.         2. PLUME REPRESENTS CONCENTRATIONS IN LAYER 3 OF THE MODEL AT AND AVERAGE ELEVATION OF APPROXIMATELY 375 FEET ABOVE MEAN SEA LEVEL.         0       500       1,000       2,000       3,000
CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER CONSULTANT YYYY-MM-DD 2019-03-12	PROJECT GROUNDWATER MODELING TITLE MODEL PREDICTED MOLYBDENUM CONCENTRATION MAP
GOLDER     PREPARED     EFT       DESIGN     JSI       REVIEW     JSI       APPROVED     MNH	YEAR 91 (2058) - CAPPED AND CLOSED SCPA           Project         Rev.         FIGURE           153-1406         0.0         A10

			Time Step: 101 Year: 2068
	SCPA		
bing		© 2019 Microsoft Corporation © 201 Distribution Airbus DS	9 DigitalGlobe @CNES (2019)
LEGEND L Sioux Energy Center Property Boundary SCPA - Unlined Bottom Ash Surface Impo	undment	NOTES 1. PLUME CONCENTRATIONS CALC MODFLOW, AND MT3DS. 2. PLUME REPRESENTS CONCENT AND MEDICAL	ULATED USING GROUNDWATER VISTAS, RATIONS IN LAYER 3 OF THE MODEL AT
Molybdenum Concentrations Greater Than Molybdenum Concentrations Greater Than Molybdenum Concentrations Greater Than	n 100 (μg/L) n 1000 (μg/L) n 3000 (μg/L)	AND AVERAGE ELEVATION OF APPF LEVEL. 0 500 1,000	2,000 3,000 Feet
CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER	<b>Ameren</b>	PROJECT GROUNDWATER MODELING	
CONSULTANT YYYY-MM- PREPARED DESIGN REVIEW	2019-03-12 D EFT JSI JSI MNH	TITLE MODEL PREDICTED MOLYBDI YEAR 101 (2068) - CAPPED AN Project 153-1406	ENUM CONCENTRATION MAP ID CLOSED SCPA Rev. FIGURE 0.0 A11

		Time Step: 111 Year: 2078
SCPA		
bing LEGEND	© 2019 Microsoft Corporation © 2019 Digit Distribution Airbus DS NOTES 1 PLUME CONCENTRATIONS CALCULATED	alGlobe OCNES (2019)
Sioux Energy Center Property Boundary	MODFLOW, AND MT3DS. 2. PLUME REPRESENTS CONCENTRATION	NS IN LAYER 3 OF THE MODEL AT
Molybdenum Concentrations Greater Than 100 (µg/L)	LEVEL. 0 500 1,000 2,0	000 3,000
Molybdenum Concentrations Greater Than 3000 (µg/L)		Feet
	PROJECT GROUNDWATER MODELING	
SIOUX ENERGY CENTER AMORTO 2019-03-12	TITLE	
PREPARED EFT	MODEL PREDICTED MOLYBDENUM YEAR 111 (2078) - CAPPED AND CLO	CONCENTRATION MAP
BULDER DESIGN JSI REVIEW JSI	Project	Rev. FIGURE
APPROVED MNH	153-1406	0.0 <b>A12</b>

	Time S       Years 2	itep: 121 088
The former of th		
The formation of the fo	© 2019 Microsoft Corporation © 2019 DigitalGlobe @CNES	(2019)
LEGEND	NOTES 1. PLUME CONCENTRATIONS CALCULATED USING GROUNE MODFLOW, AND MT3DS.	OWATER VISTAS,
SCPA - Unlined Bottom Ash Surface Impoundment	<ol> <li>PLUME REPRESENTS CONCENTRATIONS IN LAYER 3 OF AND AVERAGE ELEVATION OF APPROXIMATELY 375 FEET A LEVEL.</li> </ol>	THE MODEL AT BOVE MEAN SEA
Molybdenum Concentrations Greater Than 1000 (µg/L)	0 500 1,000 2,000	3,000
Molybdenum Concentrations Greater Than 3000 (µg/L) CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER	PROJECT GROUNDWATER MODELING	
CONSULTANT YYYY-MM-DD 2019-03-12 PREPARED EFT DESIGN JSI	MODEL PREDICTED MOLYBDENUM CONCENTRAT YEAR 121 (2088) - CAPPED AND CLOSED SCPA	ION MAP
REVIEW JSI APPROVED MNH	Project Rev. 153-1406 0.0	FIGURE A13

	Time Step: 131 Year: 2098
	© 2019 Microsoft Corporation © 2019 DigitalGlobe @CNES (2019) Distribution Airbus DS
LEGEND Sioux Energy Center Property Boundary SCPA - Unlined Bottom Ash Surface Impoundment Molybdenum Concentrations Greater Than 100 (µg/L)	NOTES 1. PLUME CONCENTRATIONS CALCULATED USING GROUNDWATER VISTAS, MODFLOW, AND MT3DS. 2. PLUME REPRESENTS CONCENTRATIONS IN LAYER 3 OF THE MODEL AT AND AVERAGE ELEVATION OF APPROXIMATELY 375 FEET ABOVE MEAN SEA LEVEL.
Molybdenum Concentrations Greater Than 1000 (μg/L)	0 500 1,000 2,000 3,000 Feet
CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER CONSULTANT YYYY-MM-DD 2019-03-12	PROJECT GROUNDWATER MODELING TITLE MODEL PREDICTED MOLYBDENUM CONCENTRATION MAP
Image: scale of the scale o	YEAR 131 (2098) - CAPPED AND CLOSED SCPA       Project     Rev.       153-1406     0.0

		Time Step: 141 Year: 2108
SCPA JOD		
LEGEND Sioux Energy Center Property Boundary	© 2019 Microsoft Corporation © 2019 Digit Distribution Airbus DS NOTES 1. PLUME CONCENTRATIONS CALCULATER MODFLOW, AND MT3DS.	alGlobe OCNES (2019)
SCPA - Unlined Bottom Ash Surface Impoundment	2. PLUME REPRESENTS CONCENTRATION AND AVERAGE ELEVATION OF APPROXIMA	NS IN LAYER 3 OF THE MODEL AT ATELY 375 FEET ABOVE MEAN SEA
Molybdenum Concentrations Greater Than 100 (µg/L)	0 500 1,000 2,0	3,000
Molybdenum Concentrations Greater Than 3000 (µg/L)		Feet
CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER	PROJECT GROUNDWATER MODELING	
CONSULTANT YYYY-MM-DD 2019-03-12 PREPARED EFT PREPARED	MODEL PREDICTED MOLYBDENUM YEAR 141 (2108) - CAPPED AND CLO	CONCENTRATION MAP
REVIEW JSI	Project	Rev. FIGURE
APPROVED MNH	153-1406	0.0 <b>A15</b>

-==



<form></form>			Time Step: 161 Year: 2128
LEEMD       Output	SCPA 1000		
Distribution       Superior       Distribution       Distributio			
Molybdenum Concentrations Greater Than 1000 (µg/L)       Molybdenum Concentrations Greater Than 3000 (µg/L)         Molybdenum Concentrations Greater Than 3000 (µg/L)       0       500       1,000       2,000       3,000         CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER       Image: Consultant       Image	LEGEND Sioux Energy Center Property Boundary SCPA - Unlined Bottom Ash Surface Impoundment Molybdenum Concentrations Greater Than 100 (ug/l )	Distribution Airbus DS NOTES 1. PLUME CONCENTRATIONS CALCULATED MODFLOW, AND MT3DS. 2. PLUME REPRESENTS CONCENTRATION AND AVERAGE ELEVATION OF APPROXIMA LEVEL	D USING GROUNDWATER VISTAS, IS IN LAYER 3 OF THE MODEL AT TELY 375 FEET ABOVE MEAN SEA
Molybdenum Concentrations Greater Than 3000 (µg/L)         CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER       Image: Colspan="2">Feet         VYYY-MM-DD       2019-03-12       PROJECT GROUNDWATER MODELING         VYYY-MM-DD       2019-03-12       Image: Colspan="2">Image: Colspan="2">Image: Colspan="2">Image: Colspan="2">Image: Colspan="2">Image: Colspan="2">Feet         VYYY-MM-DD       2019-03-12       PREPARED       EFT       Image: Colspan="2">Image: Colspan="2">Image: Colspan="2">Image: Colspan="2">Image: Colspan="2">Image: Colspan="2">Image: Colspan="2">Feet         CONSULTANT       VYY-MM-DD       2019-03-12       PROJECT       Colspan="2">Image: Colspan="2" Image: Colspa="2" Image: Colspan="2" Image: Colspan="2" Im	Molybdenum Concentrations Greater Than 1000 (µg/L)	0 500 1,000 2,0	3,000
CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER CONSULTANT VYYY-MM-DD 2019-03-12 PREPARED EFT DESIGN JSI REVIEW JSI APPROVED MNH PROJECT GROUNDWATER MODELING TITLE MODEL PREDICTED MOLYBDENUM CONCENTRATION MAP YEAR 161 (2128) - CAPPED AND CLOSED SCPA Project 153-1406 0.0 FIGURE	Molybdenum Concentrations Greater Than 3000 (µg/L)		Feet
SIOUX ENERGY CENTER     YYYY-MM-DD     2019-03-12       CONSULTANT     YYYY-MM-DD     2019-03-12       PREPARED     EFT       DESIGN     JSI       REVIEW     JSI       APPROVED     MNH	AMEREN MISSOURI	PROJECT GROUNDWATER MODELING	
REVIEW JSI Project Rev. FIGURE APPROVED MNH 153-1406 0.0 A17	SIOUX ENERGY CENTER     ***American       CONSULTANT     YYYY-MM-DD     2019-03-12       PREPARED     EFT       DESIGN     JSI	TITLE MODEL PREDICTED MOLYBDENUM YEAR 161 (2128) - CAPPED AND CLO	CONCENTRATION MAP DSED SCPA
	REVIEW JSI APPROVED MNH	Project 153-1406	Rev. FIGURE 0.0 <b>A17</b>

-==

<form></form>			Time Step: 171 Year: 2138
Distribution       © 2019 Microsoft Corporation       © 2019 DigitalGlobe       © CONES (2019)         Distribution Airbus DS       Distribution Airbus DS         LEGEND       Sioux Energy Center Property Boundary       NOTES         SCPA - Unlined Bottom Ash Surface Impoundment       Nolybdenum Concentrations Greater Than 100 (µg/L)       Nolybdenum Concentrations Greater Than 100 (µg/L)         Molybdenum Concentrations Greater Than 3000 (µg/L)       0 500 1,000 2,000 3,000         CLIENT       Molybdenum Concentrations Greater Than 3000 (µg/L)         CLIENT       MOSULANT         CONSULTANT       YYY-MM-DD         YYY-MM-DD       2019-03-12         PROJECT       GROUNDWATER MODELING         CONSULTANT       YYY-MM-DD         YYY-MM-DD       2019-03-12         PREPARED       EFT         DESIGN       JSI         REVIEW       JSI         APPROVED       MNH			
Stody Energy Center Property Boundary       MODELOW, AND MT3DS.         SCPA - Unlined Bottom Ash Surface Impoundment       MOlybdenum Concentrations Greater Than 100 (µg/L)         Molybdenum Concentrations Greater Than 1000 (µg/L)       Molybdenum Concentrations Greater Than 3000 (µg/L)         Molybdenum Concentrations Greater Than 3000 (µg/L)       MOlybdenum Concentrations Greater Than 3000 (µg/L)         CLIENT       MISSOURI         SIOUX ENERGY CENTER       MODELOW, AND MT3DS.         CONSULTANT       YYYY-MM-DD         YYYY-MM-DD       2019-03-12         PREPARED       EFT         DESIGN       JSI         REVIEW       JSI         REVIEW       JSI         APPROVED       MNH	LEGEND	© 2019 Microsoft Corporation © 2019 Digital Distribution Airbus DS NOTES 1. PLUME CONCENTRATIONS CALCULATED	IGIODE CONES (2019)
Molybdenum Concentrations Greater Than 100 (µg/L) Molybdenum Concentrations Greater Than 1000 (µg/L) Molybdenum Concentrations Greater Than 3000 (µg/L) CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER CONSULTANT VYYY-MM-DD 2019-03-12 PREPARED EFT DESIGN JSI REVIEW JSI REVIEW JSI APPROVED MNH LEVEL. 0 500 1,000 2,000 3,000 PROJECT GROUNDWATER MODELING TITLE MODEL PREDICTED MOLYBDENUM CONCENTRATION MAP YEAR 171 (2138) - CAPPED AND CLOSED SCPA Project 153-1406 PROJECT GROUNDWATER MODELING	SCPA - Unlined Bottom Ash Surface Impoundment	MODFLOW, AND MT3DS. 2. PLUME REPRESENTS CONCENTRATIONS AND AVERAGE ELEVATION OF APPROXIMAT	S IN LAYER 3 OF THE MODEL AT ELY 375 FEET ABOVE MEAN SEA
Molybdenum Concentrations Greater Than 3000 (µg/L)       Feet         CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER       Image: Consultant       Imag	Molybdenum Concentrations Greater Than 100 (μg/L) Molybdenum Concentrations Greater Than 1000 (μg/L)	0 500 1,000 2,00	3,000
CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER       YYYY-MM-DD       2019-03-12       PROJECT GROUNDWATER MODELING         CONSULTANT       YYYY-MM-DD       2019-03-12       TITLE         PREPARED       EFT       MODEL PREDICTED MOLYBDENUM CONCENTRATION MAP YEAR 171 (2138) - CAPPED AND CLOSED SCPA         REVIEW       JSI       Project       Rev.       FIGURE 153-1406	Molybdenum Concentrations Greater Than 3000 (µg/L)		Feet
CONSULTANT       YYYY-MM-DD       2019-03-12       TITLE         PREPARED       EFT       MODEL PREDICTED MOLYBDENUM CONCENTRATION MAP         DESIGN       JSI       REVIEW       JSI         REVIEW       JSI       Project       Rev.         APPROVED       MNH       153-1406       0.0       A18	CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER	PROJECT GROUNDWATER MODELING	
REVIEWJSIProjectRev.FIGUREAPPROVEDMNH153-14060.0A18	CONSULTANT     YYYY-MM-DD     2019-03-12       PREPARED     EFT       DESIGN     JSI	MODEL PREDICTED MOLYBDENUM C YEAR 171 (2138) - CAPPED AND CLOS	CONCENTRATION MAP
	REVIEW JSI APPROVED MNH	Project 153-1406	Rev. FIGURE 0.0 <b>A18</b>

-==

		Time Step: 181 Year: 2148
LEGEND Sioux Energy Center Property Boundary	Distribution Airbus DS NOTES 1. PLUME CONCENTRATIONS CALCULATED MODFLOW, AND MT3DS.	D USING GROUNDWATER VISTAS,
SCPA - Unlined Bottom Ash Surface Impoundment	2. PLUME REPRESENTS CONCENTRATION AND AVERAGE ELEVATION OF APPROXIMA	IS IN LAYER 3 OF THE MODEL AT TELY 375 FEET ABOVE MEAN SEA
Molybdenum Concentrations Greater Than 1000 (µg/L)	0 500 1,000 2,0	3,000
Molybdenum Concentrations Greater Than 3000 (µg/L)		Feet
AMEREN MISSOURI	PROJECT GROUNDWATER MODELING	
SIOUX ENERGY CENTER		
PREPARED EFT	MODEL PREDICTED MOLYBDENUM YEAR 181 (2148) - CAPPED AND CL	CONCENTRATION MAP
	Proiect	Rev. FIGURE
APPROVED MNH	153-1406	0.0 <b>A19</b>

	Time Step: 191 Year: 2158
SCPA	Public de la constant
LEGEND	NOTES 1. PLUME CONCENTRATIONS CALCULATED USING GROUNDWATER VISTAS, MODFLOW, AND MT3DS. 2. PLUME REPRESENTS CONCENTRATIONS IN LAYER 3 OF THE MODEL AT
Molybdenum Concentrations Greater Than 100 (μg/L)	AND AVERAGE ELEVATION OF APPROXIMATELY 375 FEET ABOVE MEAN SEA LEVEL. 0 500 1 000 2 000 3 000
Molybdenum Concentrations Greater Than 1000 (µg/L)	Feet
CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER	PROJECT GROUNDWATER MODELING
YYYY-MM-DD         2019-03-12           PREPARED         EFT	MODEL PREDICTED MOLYBDENUM CONCENTRATION MAP YEAR 191 (2158) - CAPPED AND CLOSED SCPA
REVIEW JSI	Project Rev. FIGURE
APPROVED MNH	153-1406 0.0 <b>A20</b>

	Time Step: 201 Year: 2168
SCPA Modeling to the second s	
bing	© 2019 Microsoft Corporation © 2019 DigitalGlobe ©CNES (2019) Distribution Airbus DS
LEGEND Sioux Energy Center Property Boundary SCPA - Unlined Bottom Ash Surface Impoundment Molybdenum Concentrations Greater Than 100 (µg/L) Molybdenum Concentrations Greater Than 1000 (µg/L)	NOTES         1. PLUME CONCENTRATIONS CALCULATED USING GROUNDWATER VISTAS, MODFLOW, AND MT3DS.         2. PLUME REPRESENTS CONCENTRATIONS IN LAYER 3 OF THE MODEL AT AND AVERAGE ELEVATION OF APPROXIMATELY 375 FEET ABOVE MEAN SEA LEVEL.         0       500       1,000       2,000       3,000
Molybdenum Concentrations Greater Than 3000 (µg/L) CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER CONSULTANT YYYY-MM-DD 2019-03-12 DDEPADED EET	PROJECT GROUNDWATER MODELING TITLE MODEL PREDICTED MOLYBDENUM CONCENTRATION MAP
GOLDER     Design     JSI       REVIEW     JSI       APPROVED     MNH	YEAR 201 (2168) - CAPPED AND CLOSED SCPA           Project         Rev.         FIGURE           153-1406         0.0         A21



	Time Step: 221 Year: 2188
SCPA 1000	
bing	© 2019 Microsoft Corporation © 2019 DigitalGlobe @CNES (2019) Distribution Airbus DS
LEGEND Sioux Energy Center Property Boundary SCPA - Unlined Bottom Ash Surface Impoundment Molybdenum Concentrations Greater Than 100 (µg/L)	NOTES1. PLUME CONCENTRATIONS CALCULATED USING GROUNDWATER VISTAS, MODFLOW, AND MT3DS.2. PLUME REPRESENTS CONCENTRATIONS IN LAYER 3 OF THE MODEL AT AND AVERAGE ELEVATION OF APPROXIMATELY 375 FEET ABOVE MEAN SEA LEVEL.05001,0002,0003,000
Molybdenum Concentrations Greater Than 1000 (µg/L)         CLIENT         AMEREN MISSOURI         SIOUX ENERGY CENTER         CONSULTANT         YYYY-MM-DD         2019-03-12	PROJECT GROUNDWATER MODELING
COLDER     PREPARED     EFT       DESIGN     JSI       REVIEW     JSI       APPROVED     MNH	MODEL PREDICTED MOLYBDENUM CONCENTRATION MAP YEAR 221 (2188) - CAPPED AND CLOSED SCPA       Project     Rev.     FIGURE       153-1406     0.0     A23
	Time Step: 231 Year: 2198
--	---
SCPA	• 219 Mircsoft Corporation 9:2019 DigitalGibble @CNES (2019)
LEGEND Sioux Energy Center Property Boundary	NOTES 1. PLUME CONCENTRATIONS CALCULATED USING GROUNDWATER VISTAS, MODFLOW, AND MT3DS. 2. PLUME REPRESENTS CONCENTRATIONS IN LAYER 3 OF THE MODEL AT
Molybdenum Concentrations Greater Than 100 (µg/L)	AND AVERAGE ELEVATION OF APPROXIMATELY 375 FEET ABOVE MEAN SEA LEVEL.
Molybdenum Concentrations Greater Than 1000 (µg/L)	
Molybdenum Concentrations Greater Than 3000 (µg/L)	
CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER	
CONSULTANT         YYYY-MM-DD         2019-03-12           PREPARED         EFT           DESIGN         COL	MODEL PREDICTED MOLYBDENUM CONCENTRATION MAP YEAR 231 (2198) - CAPPED AND CLOSED SCPA
	Project Rev. FIGURE
APPROVED MNH	153-1406 0.0 <b>A24</b>

THE DEFINITION OF THE DEFINITI	
The Area of the Ar	
© 2019 Microsoft Corporation © 2019 DigitalGlobe ©CN Distribution Airbus DS	IES (2019)
LEGEND       NOTES         Legend       1. PLUME CONCENTRATIONS CALCULATED USING GROUMODFLOW, AND MT3DS.         Score       Score         Score       Vertice         Score       Score         Score       Score         Notes       Score         Score       Score	UNDWATER VISTAS, OF THE MODEL AT
Molybdenum Concentrations Greater Than 100 (μg/L) Molybdenum Concentrations Greater Than 100 (μg/L) Δ Σου 1 000 2 000	
Molybdenum Concentrations Greater Than 1000 (μg/L)	Feet
CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER	
YYYY-MM-DD     2019-03-12       PREPARED     EFT       PREPARED     EFT       PERFORM     Interform	RATION MAP
Notesting         Notesting <t< td=""><td>FIGURE A25</td></t<>	FIGURE A25

AMEREN\_00004083

	Image: Descent and the second and the secon
The rest of the re	© 2019 Microsoft Corporation © 2019 DigitalGlobe @CNES (2019)
LEGEND Sioux Energy Center Property Boundary SCPA - Unlined Bottom Ash Surface Impoundment Molybdenum Concentrations Greater Than 100 (µg/L)	Distribution Airbus DS NOTES 1. PLUME CONCENTRATIONS CALCULATED USING GROUNDWATER VISTAS, MODFLOW, AND MT3DS. 2. PLUME REPRESENTS CONCENTRATIONS IN LAYER 3 OF THE MODEL AT AND AVERAGE ELEVATION OF APPROXIMATELY 375 FEET ABOVE MEAN SEA LEVEL.
Molybdenum Concentrations Greater Than 1000 (μg/L)	
Molybdenum Concentrations Greater Than 3000 (µg/L) CLIENT AMEREN MISSOURI SIOUX ENERGY CENTER	PROJECT GROUNDWATER MODELING
CONSULTANT YYYY-MM-DD 2019-03-12 PREPARED EFT DESIGN JSI	MODEL PREDICTED MOLYBDENUM CONCENTRATION MAP YEAR 251 (2218) - CAPPED AND CLOSED SCPA
REVIEW JSI APPROVED MNH	Project         Rev.         FIGURE           153-1406         0.0 <b>A26</b>

-==





AMEREN\_00004085

### Appendix C: Speciation Modeling

Parameter	Units	S-AM-1D	S-AM-1S	S-BMW-1D
Sampling Date		Nov-18	Nov-18	Nov-18
Charge Balance		-1.2	-4.1	4.0
pН	S.U.	7.25	7.09	7.63
Eh	mV	201	296	154
Alkalinity	mg/L as CaCO <sub>3</sub>	250	260	399
As	mg/L	0.000290	0.00130	0.000200
В	mg/L	11.7	0.432	0.140
Ва	mg/L	0.244	0.112	0.297
Са	mg/L	75.0	67.5	128
Cd	mg/L	0.000120	0.000055	0.000016
CI	mg/L	20.7	21.8	5.50
Со	mg/L	0.000435	0.00150	0.000435
Cr	mg/L	0.000039	0.000039	0.000039
F	mg/L	0.450	0.600	0.290
Fe	mg/L	3.34	1.71	9.75
K	mg/L	8.08	10.2	2.54
Li	mg/L	0.0326	0.0193	0.0162
Mg	mg/L	16.1	14.4	25.9
Mn	mg/L	0.389	0.576	1.09
Mo	mg/L	0.446	0.0580	0.000450
Na	mg/L	21.6	17.3	6.56
Р	mg/L-P	0.0913	0.222	0.114
SO <sub>4</sub>	mg/L	40.1	11.4	13.3
MINERAL PHASES	- Saturation Indices (a)			
Ferrihydrite	Fe(OH) <sub>3</sub>	3.9	3.5	4.7
Siderite	FeCO <sub>3</sub>	-1.0	-1.4	-0.7
Melanterite	FeSO₄ 7H₂O	-6.9	-7.7	-7.6
Rhodochrosite	MnCO <sub>3</sub>	-0.3	-0.3	0.6
Birnessite	MnO <sub>2</sub>	-13.6	-10.9	-13.4
Manganite	MnOOH	-5.6	-4.3	-4.8
Gypsum	CaSO <sub>4</sub> :2H <sub>2</sub> O	-1.9	-2.5	-2.3
Jarosite-H	(H <sub>3</sub> O)Fe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	-2.9	-4.7	-3.3
Jarosite-K	KFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	3.9	2.0	3.5
Jarosite-Na	NaFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	0.8	-1.2	0.4
Calcite	CaCO <sub>3</sub>	0.0	-0.2	0.7
Magnesite	MgCO <sub>3</sub>	-1.3	-1.5	-0.6
Barite	BaSO <sub>4</sub>	0.6	-0.3	0.1
Witherite	BaCO <sub>3</sub>	-2.9	-3.3	-2.2
Fluorite	CaF <sub>2</sub>	-1.8	-1.5	-2.0
Carbon Dioxide	pCO <sub>2</sub> (g) (b)	-1.8	-1.7	-2.1

## Notes:

Non-detect values equal 1/2 analytical detection limit Redox converted from field ORP to Eh by +200 mV  $\,$ 

<sup>(a)</sup> Saturation indices between -0.5 and 0.5 identified by bold type and grey shading

### Appendix C: Speciation Modeling

Parameter	Units	S-BMW-3D	S-UMW-1D	S-UMW-2D
Sampling Date		Nov-18	Nov-18	Nov-18
Charge Balance		0.4	2.7	-8.5
рН	s.u.	7.60	7.60	8.28
Eh	mV	201	101	29.6
Alkalinity	mg/L as CaCO <sub>3</sub>	350	204	116
As	mg/L	0.0000325	0.00140	0.00280
В	mg/L	0.0473	0.163	18.4
Ва	mg/L	0.645	0.134	0.0657
Са	mg/L	108	75.3	175
Cd	mg/L	0.000016	0.000016	0.000290
CI	mg/L	8.40	21.8	20.0
Co	mg/L	0.000435	0.000435	0.000435
Cr	mg/L	0.000039	0.000039	0.000039
	mg/L	0.300	0.190	0.460
Fe	mg/L	7.68	0.846	0.266
K	mg/L	3.64	5.49	23.9
	mg/L	0.0254	0.0157	0.0234
Mp	mg/L	23.0	21.3	• 0.102
Mo	mg/L	0.459	0.114	0.165
Na	mg/L	6.50	15.2	50.0
P	mg/L_P	0.30	0.0587	0.0284
<u>s</u> 0.	mg/L	27.5	63.4	522
	- Saturation Indices (a)	21.0	00.4	022
Ferrihydrite	Fe(OH) <sub>3</sub>	4.5	3.8	3.6
Siderite	FeCO <sub>3</sub>	-1.0	-2.2	-2.1
Melanterite	FeSO₄ 7H₂O	-7.6	-8.4	-7.6
Rhodochrosite	MnCO <sub>3</sub>	0.2	-0.6	-0.2
Birnessite	MnO <sub>2</sub>	-12.3	-15.9	-15.8
Manganite	MnOOH	-4.5	-6.8	-5.8
Gypsum	CaSO <sub>4</sub> :2H <sub>2</sub> O	-2.0	-1.8	-0.7
Jarosite-H	(H <sub>3</sub> O)Fe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	-2.9	-4.2	-5.8
Jarosite-K	KFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	4.1	2.5	2.4
Jarosite-Na	NaFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	0.8	-0.4	-0.7
Calcite	CaCO₃	0.6	0.3	0.8
Magnesite	MgCO <sub>3</sub>	-0.7	-1.0	-1.3
Barite	BaSO <sub>4</sub>	0.8	0.4	1.0
Witherite	BaCO <sub>3</sub>	-2.0	-2.8	-2.9
Fluorite	CaF <sub>2</sub>	-2.0	-2.6	-1.5
Carbon Dioxide	pCO <sub>2</sub> (g) (b)	-2.1	-2.3	-3.3

# Notes:

Non-detect values equal 1/2 analytical detection limit Redox converted from field ORP to Eh by +200 mV  $\,$ 

<sup>(a)</sup> Saturation indices between -0.5 and 0.5 identified by bold type and grey shading

## Appendix C: Speciation Modeling

Parameter	Units	S-UMW-3D	S-UMW-4D	S-UMW-5D
Sampling Date		Nov-18	Nov-18	Nov-18
Charge Balance		-13.2	-8.0	-1.0
pН	S.U.	8.34	7.35	7.47
Eh	mV	23.7	65.1	11.8
Alkalinity	mg/L as CaCO <sub>3</sub>	56.7	201	264
As	mg/L	0.000820	0.000290	0.000400
В	mg/L	31.9	16.8	5.53
Ва	mg/L	0.0750	0.0569	0.265
Са	mg/L	248	153	72.7
Cd	mg/L	0.001000	0.000940	0.000054
CI	mg/L	12.8	23.8	24.9
Со	mg/L	0.000435	0.000435	0.000435
Cr	mg/L	0.000039	0.000039	0.000039
F	mg/L	0.960	0.490	0.490
Fe	mg/L	0.626	6.26	3.38
K	mg/L	20.4	13.1	9.26
	mg/L	0.0117	0.0383	0.0229
Mg	mg/L	7.21	21.6	16.7
IVIN Ma	mg/L	0.399	1.46	0.444
Mo	mg/L	4.00	3.90	0.181
Na	mg/L	0.0202	59.9	18.7
P 20	mg/L-P	0.0303	0.0040	0.0783
	Ing/L	994	459	12.0
IVIINERAL PHASES		10	4.2	
Ferrinyunite		4.0	4.3	4.1
Siderite		-2.0	-1.3	-0.6
	$FeSO_4$ / $H_2O$	-7.5	-0.3	-7.3
Rhodochrosite	MnCO <sub>3</sub>	-0.3	0.1	0.0
Birnessite	MnO <sub>2</sub>	-15.5	-17.4	-19.1
Manganite	MnOOH	-5.5	-7.1	-8.0
Gypsum	CaSO₄:2H₂O	-0.4	-0.8	-2.5
Jarosite-H	(H <sub>3</sub> O)Fe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	-4.5	-0.2	-4.2
Jarosite-K	KFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	3.8	6.9	2.9
Jarosite-Na	NaFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	1.0	4.0	-0.3
Calcite	CaCO₃	0.5	0.1	0.2
Magnesite	MgCO <sub>3</sub>	-1.7	-1.3	-1.0
Barite	BaSO <sub>4</sub>	1.2	0.8	0.1
Witherite	BaCO <sub>3</sub>	-3.3	-3.6	-2.6
Fluorite	CaF <sub>2</sub>	-0.9	-1.6	-1.7
Carbon Dioxide	pCO <sub>2</sub> (g) (b)	-3.8	-2.1	-2.0

## Notes:

Non-detect values equal 1/2 analytical detection limit Redox converted from field ORP to Eh by +200 mV  $\,$ 

<sup>(a)</sup> Saturation indices between -0.5 and 0.5 identified by bold type and grey shading

## Appendix C: Speciation Modeling

Parameter	Units	S-UMW-6D	S-BMW-1S	S-BMW-3S
Sampling Date		Nov-18	Nov-18	Nov-18
Charge Balance		1.4	2.2	0.1
pН	S.U.	6.86	7.46	7.49
Eh	mV	112	213	266
Alkalinity	mg/L as CaCO <sub>3</sub>	386	464	368
As	mg/L	0.000290	0.000950	0.000450
В	mg/L	0.589	0.0729	0.0615
Ва	mg/L	0.182	0.160	0.157
Са	mg/L	123	157	124
Cd	mg/L	0.000016	-	-
CI	mg/L	8.60	6.70	10.1
Со	mg/L	0.000435	-	-
Cr	mg/L	0.000039	-	-
F	mg/L	0.330	0.340	0.360
Fe	mg/L	8.84	0.0200	0.0630
K	mg/L	5.53	0.580	0.772
	mg/L	0.0203	0.00230	0.0121
Mg	mg/L	28.6	29.0	21.4
Mn	mg/L	0.716	0.607	0.400
Mo	mg/L	0.0528	0.00220	0.00280
	mg/L	0.147	5.60	5.07
P 80	mg/L-P	0.147	0.103	0.0750
	Ing/L	53.4	28.8	25.0
IVIINERAL PHASES		10	4 7	2.4
Ferninyante		4.0	1.7	2.4
Siderite		-1.4	-2.2	-2.2
		-7.1	-0.0	-0.0
Rhodochrosite	MINCO <sub>3</sub>	-0.3	0.3	0.0
Birnessite	MnO <sub>2</sub>	-17.9	-12.3	-10.6
Manganite	MnOOH	-8.0	-4.6	-3.8
Gypsum	CaSO <sub>4</sub> :2H <sub>2</sub> O	-1.7	-1.9	-2.0
Jarosite-H	(H <sub>3</sub> O)Fe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	-0.9	-10.7	-9.0
Jarosite-K	KFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	5.3	-4.8	-3.0
Jarosite-Na	NaFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	2.1	-7.4	-5.6
Calcite	CaCO₃	0.0	0.7	0.6
Magnesite	MgCO <sub>3</sub>	-1.3	-0.6	-0.8
Barite	BaSO <sub>4</sub>	0.4	0.1	0.1
Witherite	BaCO <sub>3</sub>	-3.2	-2.6	-2.7
Fluorite	CaF <sub>2</sub>	-1.9	-1.8	-1.8
Carbon Dioxide	pCO <sub>2</sub> (g) (b)	-1.3	-1.8	-1.9

## Notes:

Non-detect values equal 1/2 analytical detection limit Redox converted from field ORP to Eh by +200 mV  $\,$ 

<sup>(a)</sup> Saturation indices between -0.5 and 0.5 identified by bold type and grey shading

## Appendix C: Speciation Modeling

Parameter	Units	S-LMW-1S	S-LMW-2S	S-LMW-3S
Sampling Date		Nov-18	Nov-18	Nov-18
Charge Balance		1.4	0.1	0.5
pН	S.U.	7.40	6.95	6.75
Eh	mV	184	290	284
Alkalinity	mg/L as CaCO₃	227	428	529
As	mg/L	0.00200	0.00100	0.000570
В	mg/L	0.539	8.53	0.298
Ва	mg/L	0.127	0.127	0.200
Са	mg/L	79.4	197	188
Cd	mg/L	0.000049	0.000380	0.000110
CI	mg/L	42.6	174	51.3
Со	mg/L	-	-	-
Cr	mg/L	0.000039	0.000039	0.000300
F	mg/L	0.370	0.320	0.260
Fe	mg/L	0.0230	0.166	0.0190
K	mg/L	6.80	6.72	5.12
Li	mg/L	0.0210	0.0416	0.0294
Mg	mg/L	20.1	41.7	36.9
Mn	mg/L	0.0594	0.545	0.00430
Mo	mg/L	0.0436	0.709	0.00110
Na	mg/L	33.4	91.7	16.9
P	mg/L-P	0.0848	0.00815	0.00815
	mg/L	62.2	188	54.3
MINERAL PHASES	- Saturation indices (a)	10		1.0
Ferrinyarite	Fe(OH) <sub>3</sub>	1.9	2.4	1.0
Siderite		-2.4	-2.8	-2.8
Melanterite	$FeSO_4$ / $H_2O$	-8.4	-8.1	-8.6
Rhodochrosite	MnCO <sub>3</sub>	-1.0	-0.4	-2.6
Birnessite	MnO <sub>2</sub>	-14.2	-11.8	-14.9
Manganite	MnOOH	-6.2	-5.0	-7.7
Gypsum	CaSO₄:2H₂O	-1.8	-1.1	-1.6
Jarosite-H	(H <sub>3</sub> O)Fe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	-9.1	-5.3	-9.5
Jarosite-K	KFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	-2.4	1.1	-3.4
Jarosite-Na	NaFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	-5.2	-1.3	-6.4
Calcite	CaCO₃	0.1	0.2	0.1
Magnesite	MgCO <sub>3</sub>	-1.1	-1.1	-1.2
Barite	BaSO <sub>4</sub>	0.4	0.7	0.4
Witherite	BaCO <sub>3</sub>	-3.0	-3.3	-3.2
Fluorite	CaF <sub>2</sub>	-2.0	-1.8	-2.0
Carbon Dioxide	pCO <sub>2</sub> (g) (b)	-2.0	-1.3	-1.0

# Notes:

Non-detect values equal 1/2 analytical detection limit Redox converted from field ORP to Eh by +200 mV  $\,$ 

 $^{\rm (a)}$  Saturation indices between -0.5 and 0.5 identified by bold type and grey shading

## Appendix C: Speciation Modeling

Parameter	Units	S-LMW-4S	S-LMW-5S	S-LMW-6S
Sampling Date		Nov-18	Nov-18	Nov-18
Charge Balance		3.5	-5.8	-1.4
pН	S.U.	6.06	6.74	6.81
Eh	mV	166	373	397
Alkalinity	mg/L as CaCO <sub>3</sub>	540	357	430
As	mg/L	0.000540	0.000730	0.000640
В	mg/L	1.02	13.4	10.4
Ва	mg/L	0.247	0.0735	0.0455
Са	mg/L	179	280	199
Cd	mg/L	0.000170	0.00110	0.00150
CI	mg/L	2.90	27.9	2.20
Co	mg/L	-	-	-
Cr	mg/L	0.000039	0.000220	0.000039
F	mg/L	0.350	0.340	0.320
Fe	mg/L	0.0280	0.266	0.0270
K	mg/L	5.05	4.56	4.65
	mg/L	0.0389	0.0521	0.0249
Mg	mg/L	36.9	54.2	► 52.5
Mn	mg/L	0.260	1.70	0.373
Mo	mg/L	0.00210	0.690	0.00110
	mg/L	14.3	130	44.1
r s0	mg/L-P	0.00815	0.00015	0.00615
	mg/L Saturation Indicos (a)	50.0	912	385
Forribydrite		0.6	2.2	1 3
Siderite		3.5	2.3	3.0
Melanterite		-5.5	-3.2	-3.0
Phodochrosito	$M_{\rm PCO}$	-0.0	-7.0	-7.0
Rinouochiosile	MnO	-1.5	-0.3	-0.7
Mangapito		-19.9	-9.0	-9.0
Gynsum		-1.7	-5.8	-3.8
		-1.7	- <b>0.4</b>	-0.0
Jarosite-K	$(130) e_3(304)_2(01)_6$	-0.2	27	-7.4
Jarosite-Na	$N_{2}E_{0}(SO_{4})_{2}(OT)_{6}$	-2.0	0.7	-1.5
Caloita	$C_{3}(50_{4})_{2}(511)_{6}$	-5.0	0.7	-5.0
Magnosito		-0.0	-0.1	1.0
Parita		-1.9	-1.4	-1.2
Darite		0.0	2.0	0.0
Eluorito		-3.0	-3.9 1 0	-3.9
		-1./	-1.0	-1.9
Carbon Dioxide	pCO <sub>2</sub> (g) (b)	-0.3	-1.2	-1.2

# Notes:

Non-detect values equal 1/2 analytical detection limit Redox converted from field ORP to Eh by +200 mV  $\,$ 

 $^{\rm (a)}$  Saturation indices between -0.5 and 0.5 identified by bold type and grey shading

## Appendix C: Speciation Modeling

Parameter	Units	S-LMW-7S	S-LMW-8S	S-LMW-9S
Sampling Date		Nov-18	Nov-18	Nov-18
Charge Balance		1.5	0.1	-7.6
pН	S.U.	6.84	6.93	6.82
Eh	mV	326	373	243
Alkalinity	mg/L as CaCO <sub>3</sub>	391	306	415
As	mg/L	0.000450	0.00110	0.000910
В	mg/L	2.74	8.50	1.76
Ва	mg/L	0.0910	0.105	0.0734
Са	mg/L	221	177	194
Cd	mg/L	0.000260	0.000710	0.000260
CI	mg/L	11.6	38.9	278
Co	mg/L	-	-	-
Cr	mg/L	0.000039	0.000039	0.000170
F	mg/L	0.340	0.870	0.560
Fe	mg/L	0.0210	0.0146	0.126
K	mg/L	3.99	4.88	4.72
Li	mg/L	0.0221	0.0231	0.0434
Mg	mg/L	60.2	41.0	60.6
Mn	mg/L	0.118	0.488	0.583
Mo	mg/L	0.00150	0.390	0.0114
Na	mg/L	16.9	77.8	49.9
P	mg/L-P	0.00815	0.0316	0.00815
	mg/L	396	405	163
MINERAL PHASES	- Saturation indices (a)	10		
Ferrinyarite	Fe(OH) <sub>3</sub>	1.2	1.1	2.2
Siderite		-3.0	-3.0	-2.9
Melanterite	$FeSO_4$ / $H_2O$	-7.8	-7.8	-8.2
Rhodochrosite	MnCO <sub>3</sub>	-1.2	-0.6	-0.5
Birnessite	MnO <sub>2</sub>	-11.8	-9.1	-13.8
Manganite	MnOOH	-5.4	-3.7	-6.1
Gypsum	CaSO <sub>4</sub> :2H <sub>2</sub> O	-0.8	-0.8	-1.2
Jarosite-H	(H <sub>3</sub> O)Fe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	-7.8	-8.4	-5.5
Jarosite-K	KFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	-1.7	-2.2	0.5
Jarosite-Na	NaFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	-4.6	-4.5	-2.0
Calcite	CaCO <sub>3</sub>	0.1	0.0	0.1
Magnesite	MgCO <sub>3</sub>	-1.1	-1.3	-1.1
Barite	BaSO <sub>4</sub>	0.9	1.0	0.4
Witherite	BaCO <sub>3</sub>	-3.6	-3.5	-3.7
Fluorite	CaF <sub>2</sub>	-1.8	-1.0	-1.4
Carbon Dioxide	pCO <sub>2</sub> (g) (b)	-1.3	-1.5	-1.2

# Notes:

Non-detect values equal 1/2 analytical detection limit Redox converted from field ORP to Eh by +200 mV  $\,$ 

 $^{\rm (a)}$  Saturation indices between -0.5 and 0.5 identified by bold type and grey shading

### Appendix C: Speciation Modeling

Parameter	Units	S-TP-1D	S-TP-1M	S-TP-1S
Sampling Date		Nov-18	Nov-18	Nov-18
Charge Balance		-6.7	-0.3	-0.4
pН	S.U.	7.31	7.07	6.88
Eh	mV	94.7	94.7	59.2
Alkalinity	mg/L as CaCO <sub>3</sub>	187	241	438
As	mg/L	0.000160	0.000120	0.0253
В	mg/L	0.492	0.293	0.122
Ва	mg/L	0.0980	0.212	0.369
Са	mg/L	54.4	78.4	204
Cd	mg/L	0.000016	0.000016	0.000016
CI	mg/L	23.5	55.6	325
Со	mg/L	0.000435	0.000435	0.00270
Cr	mg/L	0.000110	0.000190	0.000240
F	mg/L	0.380	0.350	0.360
Fe	mg/L	2.86	6.70	22.6
К	mg/L	6.88	1.35	1.80
Li	mg/L	0.0164	0.0175	0.00650
Mg	mg/L	13.8	20.3	53.0
Mn	mg/L	0.329	0.398	11.6
Мо	mg/L	0.00350	0.00180	0.00580
Na	mg/L	17.1	38.0	71.6
P	mg/L-P	0.0913	0.218	0.652
SO <sub>4</sub>	mg/L	51. <mark>6</mark>	50.4	34.8
MINERAL PHASES	- Saturation Indices (a)			
Ferrihydrite	Fe(OH)₃	3.9	4.0	4.4
Siderite	FeCO <sub>3</sub>	-1.6	-1.3	-1.1
Melanterite	FeSO <sub>4</sub> 7H <sub>2</sub> O	-7.3	-6.9	-7.1
Rhodochrosite	MnCO <sub>3</sub>	-0.5	-0.5	0.9
Birnessite	MnO <sub>2</sub>	-17.2	-18.0	-18.6
Manganite	MnOOH	-7.2	-7.9	-7.7
Gypsum	CaSO <sub>4</sub> :2H <sub>2</sub> O	-1.9	-1.9	-1.8
Jarosite-H	(H <sub>3</sub> O)Fe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	-3.1	-1.6	-0.4
Jarosite-K	KFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	3.8	4.2	5.3
Jarosite-Na	NaFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	0.7	2.2	3.4
Calcite	CaCO <sub>3</sub>	-0.2	-0.2	0.2
Magnesite	MgCO <sub>3</sub>	-1.4	-1.4	-1.0
Barite	BaSO <sub>4</sub>	0.3	0.6	0.4
Witherite	BaCO <sub>3</sub>	-3.3	-3.1	-2.9
Fluorite	CaF <sub>2</sub>	-2.0	-2.0	-1.7
Carbon Dioxide	$pCO_2(g)(b)$	-2.0	-1.7	-1.3

# Notes:

Non-detect values equal 1/2 analytical detection limit Redox converted from field ORP to Eh by +200 mV  $\,$ 

 $^{\rm (a)}$  Saturation indices between -0.5 and 0.5 identified by bold type and grey shading

### Appendix C: Speciation Modeling

Parameter	Units	S-TP-2D	S-TP-2M	S-TP-2S
Sampling Date		Nov-18	Nov-18	Nov-18
Charge Balance		-4.6	0.6	1.0
pН	s.u.	6.11	6.15	6.22
Eh	mV	118	130	207
Alkalinity	mg/L as CaCO <sub>3</sub>	457	435	502
As	mg/L	0.000120	0.000190	0.0139
В	mg/L	0.0703	0.121	0.0805
Ва	mg/L	0.0872	0.178	0.283
Са	mg/L	274	191	151
Cd	mg/L	0.000016	0.000016	0.000016
CI	mg/L	86.6	11.4	11.5
Со	mg/L	0.000435	0.000435	0.00290
Cr	mg/L	0.000039	0.000039	0.000039
F	mg/L	0.0950	0.0950	0.0950
Fe	mg/L	17.4	16.9	12.6
К	mg/L	6.11	5.16	1.14
Li	mg/L	0.0471	0.0267	0.0132
Mg	mg/L	68.9	44.5	37.8
Mn	mg/L	1.16	0.862	4.86
Мо	mg/L	0.000450	0.000450	0.0118
Na	mg/L	20.7	18.1	12.9
P	mg/L-P	0.0913	0.0946	0.267
SO <sub>4</sub>	mg/L	520	254	50.5
MINERAL PHASES	- Saturation Indices (a)			
Ferrihydrite	Fe(OH)₃	3.4	3.4	3.4
Siderite	FeCO <sub>3</sub>	-2.8	-2.7	-2.2
Melanterite	FeSO <sub>4</sub> 7H <sub>2</sub> O	-6.8	-7.0	-7.3
Rhodochrosite	MnCO <sub>3</sub>	-1.0	-1.0	-0.1
Birnessite	MnO <sub>2</sub>	-20.9	-20.4	-16.7
Manganite	MnOOH	-10.1	-9.8	-7.5
Gypsum	CaSO₄:2H₂O	-0.6	-1.0	-1.7
Jarosite-H	(H <sub>3</sub> O)Fe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	1.9	1.4	-0.4
Jarosite-K	KFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	7.6	7.1	4.7
Jarosite-Na	NaFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	4.6	4.1	2.2
Calcite	CaCO₃	-0.6	-0.6	-0.5
Magnesite	MgCO <sub>3</sub>	-1.8	-1.9	-1.7
Barite	BaSO <sub>4</sub>	1.0	1.1	0.6
Witherite	BaCO <sub>3</sub>	-4.3	-4.0	-3.6
Fluorite	CaF <sub>2</sub>	-2.8	-2.9	-2.9
Carbon Dioxide	pCO <sub>2</sub> (g) (b)	-0.5	-0.5	-0.5

# Notes:

Non-detect values equal 1/2 analytical detection limit Redox converted from field ORP to Eh by +200 mV  $\,$ 

<sup>(a)</sup> Saturation indices between -0.5 and 0.5 identified by bold type and grey shading

### **Appendix C: Speciation Modeling**

Parameter	Units	S-TP-3D	S-TP-3M	S-TP-3S
Sampling Date		Nov-18	Nov-18	Nov-18
Charge Balance		-1.7	0.0	0.2
pН	s.u.	7.17	7.12	7.30
Eh	mV	184	219	337
Alkalinity	mg/L as $CaCO_3$	355	335	410
As	mg/L	0.000170	0.000260	0.00420
В	mg/L	0.0520	0.0482	0.0713
Ва	mg/L	0.574	0.434	0.222
Са	mg/L	119	109	113
Cd	mg/L	0.000016	0.000016	0.000033
CI	mg/L	7.60	8.40	7.20
Со	mg/L	0.000435	0.000435	0.00110
Cr	mg/L	0.000160	0.000220	0.000180
F	mg/L	0.230	0.290	0.420
Fe	mg/L	8.08	9.71	3.41
К	mg/L	4.15	4.21	6.37
Li	mg/L	0.0321	0.0210	0.0119
Mg	mg/L	28.1	23.9	22.2
Mn	mg/L	0.603	0.600	1.81
Мо	mg/L	0.000450	0.00120	0.0308
Na	mg/L	7.44	12.0	30.2
Р	mg/L-P	0.114	0.0880	0.00815
SO <sub>4</sub>	mg/L	87.5	62.5	30.4
MINERAL PHASES	- Saturation Indices (a)			
Ferrihydrite	Fe(OH)₃	4.1	4.2	3.9
Siderite	FeCO <sub>3</sub>	-1.5	-1.4	-0.8
Melanterite	FeSO <sub>4</sub> 7H <sub>2</sub> O	-7.1	-7.1	-7.1
Rhodochrosite	MnCO <sub>3</sub>	-0.1	-0.2	0.5
Birnessite	MnO <sub>2</sub>	-14.6	-13.6	-8.3
Manganite	MnOOH	-6.0	-5.5	-2.5
Gypsum	CaSO <sub>4</sub> :2H <sub>2</sub> O	-1.5	-1.7	-2.0
Jarosite-H	(H <sub>3</sub> O)Fe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	-1.4	-1.4	-3.5
Jarosite-K	KFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	5.2	5.2	3.3
Jarosite-Na	NaFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	1.9	2.1	0.5
Calcite	CaCO₃	0.2	0.1	0.4
Magnesite	MgCO <sub>3</sub>	-1.0	-1.2	-0.9
Barite	BaSO <sub>4</sub>	1.2	1.0	0.3
Witherite	BaCO <sub>3</sub>	-2.5	-2.7	-2.7
Fluorite	CaF <sub>2</sub>	-2.2	-2.0	-1.7
Carbon Dioxide	pCO <sub>2</sub> (g) (b)	-1.6	-1.6	-1.7

# Notes:

Non-detect values equal 1/2 analytical detection limit Redox converted from field ORP to Eh by +200 mV  $\,$ 

<sup>(a)</sup> Saturation indices between -0.5 and 0.5 identified by bold type and grey shading <sup>(b)</sup>  $pCO_2(g)$  values presented at  $10^{\text{value}}$  atmospheres

### Appendix C: Speciation Modeling

Parameter	Units	S-TP-4D	S-TP-4M	S-TP-4S
Sampling Date		Nov-18	Nov-18	Nov-18
Charge Balance		-1.1	1.0	-0.6
pН	s.u.	7.14	7.15	7.15
Eh	mV	260	349	414
Alkalinity	mg/L as CaCO <sub>3</sub>	305	337	366
As	mg/L	0.000950	0.000330	0.00580
В	mg/L	0.0565	0.0730	0.112
Ва	mg/L	0.557	0.408	0.192
Са	mg/L	104	112	90.7
Cd	mg/L	0.000016	0.000016	0.000016
CI	mg/L	8.30	6.10	30.9
Со	mg/L	0.000435	0.000435	0.00140
Cr	mg/L	0.000160	0.000210	0.000039
F	mg/L	0.310	0.370	0.350
Fe	mg/L	6.56	7.15	1.91
К	mg/L	3.11	4.06	5.73
Li	mg/L	0.0296	0.0249	0.0148
Mg	mg/L	25.6	25.0	19.5
Mn	mg/L	0.438	0.605	2.18
Мо	mg/L	0.000450	0.00180	0.0331
Na	mg/L	6.62	9.80	59.7
Р	mg/L-P	0.0978	0.0783	0.00815
SO <sub>4</sub>	mg/L	78. <mark>4</mark>	60.4	43.0
MINERAL PHASES	- Saturation Indices (a)			
Ferrihydrite	Fe(OH)₃	4.1	4.1	3.6
Siderite	FeCO <sub>3</sub>	-0.9	-1.2	-2.5
Melanterite	FeSO <sub>4</sub> 7H <sub>2</sub> O	-6.5	-7.0	-8.5
Rhodochrosite	MnCO <sub>3</sub>	-0.3	-0.2	0.4
Birnessite	MnO <sub>2</sub>	-12.1	-8.9	-6.1
Manganite	MnOOH	-4.9	-3.2	-1.6
Gypsum	CaSO <sub>4</sub> :2H <sub>2</sub> O	-1.6	-1.7	-1.9
Jarosite-H	(H <sub>3</sub> O)Fe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	-1.5	-1.6	-3.5
Jarosite-K	KFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	4.8	4.8	3.1
Jarosite-Na	NaFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	1.6	1.7	0.6
Calcite	CaCO₃	0.1	0.1	0.1
Magnesite	MgCO <sub>3</sub>	-1.2	-1.1	-1.2
Barite	BaSO <sub>4</sub>	1.2	0.9	0.4
Witherite	BaCO <sub>3</sub>	-2.5	-2.6	-2.9
Fluorite	CaF <sub>2</sub>	-2.0	-1.8	-1.9
Carbon Dioxide	pCO <sub>2</sub> (g) (b)	-1.7	-1.6	-1.6

# Notes:

Non-detect values equal 1/2 analytical detection limit Redox converted from field ORP to Eh by +200 mV  $\,$ 

<sup>(a)</sup> Saturation indices between -0.5 and 0.5 identified by bold type and grey shading

### Appendix C: Speciation Modeling

Parameter	Units	S-TP-5D	S-TP-5M	S-TP-5S
Sampling Date		Nov-18	Nov-18	Nov-18
Charge Balance		1.7	2.8	-0.9
pН	s.u.	7.11	7.15	7.29
Eh	mV	118	130	172
Alkalinity	mg/L as CaCO₃	275	318	430
As	mg/L	0.000300	0.00350	0.00370
В	mg/L	5.46	3.19	0.263
Ва	mg/L	0.183	0.252	0.440
Са	mg/L	141	149	124
Cd	mg/L	0.000056	0.000016	0.000040
CI	mg/L	26.8	8.90	47.7
Со	mg/L	0.000435	0.000435	0.000950
Cr	mg/L	0.000039	0.000039	0.000039
F	mg/L	0.340	0.300	0.280
Fe	mg/L	10.3	8.53	4.36
К	mg/L	5.16	5.62	5.23
Li	mg/L	0.0330	0.0310	0.00230
Mg	mg/L	32.4	26.5	27.4
Mn	mg/L	0.993	0.360	1.12
Мо	mg/L	0.175	0.0128	0.0317
Na	mg/L	24.8	17.2	30.0
Р	mg/L-P	0.101	0.0652	0.0176
SO <sub>4</sub>	mg/L	218	170	11.3
MINERAL PHASES	- Saturation Indices (a)			
Ferrihydrite	Fe(OH) <sub>3</sub>	4.2	4.2	4.0
Siderite	FeCO <sub>3</sub>	-1.7	-2.0	-0.7
Melanterite	FeSO <sub>4</sub> 7H <sub>2</sub> O	-6.9	-7.4	-7.5
Rhodochrosite	MnCO <sub>3</sub>	-0.1	-0.5	0.3
Birnessite	MnO <sub>2</sub>	-16.8	-16.6	-14.1
Manganite	MnOOH	-7.1	-7.2	-5.5
Gypsum	CaSO₄:2H₂O	-1.1	-1.2	-2.4
Jarosite-H	(H <sub>3</sub> O)Fe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	-0.1	-0.6	-3.9
Jarosite-K	KFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	6.4	6.0	2.8
Jarosite-Na	NaFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	3.6	3.0	0.0
Calcite	CaCO <sub>3</sub>	0.0	0.2	0.4
Magnesite	MgCO <sub>3</sub>	-1.2	-1.2	-0.9
Barite	BaSO <sub>4</sub>	1.1	1.1	0.2
Witherite	BaCO <sub>3</sub>	-3.1	-2.9	-2.4
Fluorite	CaF <sub>2</sub>	-1.9	-1.9	-2.0
Carbon Dioxide	pCO <sub>2</sub> (g) (b)	-1.7	-1.7	-1.7

# Notes:

Non-detect values equal 1/2 analytical detection limit Redox converted from field ORP to Eh by +200 mV  $\,$ 

 $^{\rm (a)}$  Saturation indices between -0.5 and 0.5 identified by bold type and grey shading

### Appendix C: Speciation Modeling

Parameter	Units	S-TP-6D	S-TP-6M	S-TP-6S
Sampling Date		Nov-18	Nov-18	Nov-18
Charge Balance		-0.7	0.2	-1.3
pН	s.u.	6.34	6.42	6.23
Eh	mV	136	172	266
Alkalinity	mg/L as CaCO₃	353	386	376
As	mg/L	0.000170	0.000520	0.00200
В	mg/L	0.0704	0.0638	0.104
Ва	mg/L	0.391	0.454	0.224
Са	mg/L	121	132	121
Cd	mg/L	0.000016	0.000034	0.000016
CI	mg/L	13.3	14.3	6.70
Со	mg/L	0.000435	0.000435	0.00120
Cr	mg/L	0.000039	0.000039	0.000039
F	mg/L	0.0950	0.260	0.270
Fe	mg/L	9.09	10.2	1.02
К	mg/L	4.09	4.13	3.45
Li	mg/L	0.0280	0.0228	0.0337
Mg	mg/L	28.6	27.0	24.6
Mn	mg/L	0.472	0.452	0.615
Мо	mg/L	0.00200	0.00290	0.00430
Na	mg/L	6.23	16.3	7.87
Р	mg/L-P	0.104	0.0391	0.0280
SO <sub>4</sub>	mg/L	78.5	80.4	50.0
MINERAL PHASES	- Saturation Indices (a)			
Ferrihydrite	Fe(OH)₃	3.4	3.5	2.4
Siderite	FeCO <sub>3</sub>	-2.2	-2.1	-2.5
Melanterite	FeSO <sub>4</sub> 7H <sub>2</sub> O	-7.1	-7.1	-7.6
Rhodochrosite	MnCO <sub>3</sub>	-1.1	-1.0	-1.0
Birnessite	MnO <sub>2</sub>	-19.6	-18.1	-15.4
Manganite	MnOOH	-9.4	-8.5	-7.4
Gypsum	CaSO <sub>4</sub> :2H <sub>2</sub> O	-1.5	-1.5	-1.7
Jarosite-H	(H <sub>3</sub> O)Fe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	-0.4	-0.3	-3.4
Jarosite-K	KFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	5.3	5.5	2.1
Jarosite-Na	NaFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	2.0	2.6	-1.1
Calcite	CaCO <sub>3</sub>	-0.6	-0.5	-0.7
Magnesite	MgCO <sub>3</sub>	-1.9	-1.8	-2.0
Barite	BaSO <sub>4</sub>	1.0	1.0	0.5
Witherite	BaCO <sub>3</sub>	-3.5	-3.3	-3.8
Fluorite	CaF <sub>2</sub>	-3.0	-2.1	-2.1
Carbon Dioxide	pCO <sub>2</sub> (g) (b)	-0.8	-0.9	-0.7

# Notes:

Non-detect values equal 1/2 analytical detection limit Redox converted from field ORP to Eh by +200 mV  $\,$ 

 $^{\rm (a)}$  Saturation indices between -0.5 and 0.5 identified by bold type and grey shading

### Appendix C: Speciation Modeling

Parameter	Units	S-TP-7D	S-TP-7M	S-TP-7S
Sampling Date		Nov-18	Nov-18	Nov-18
Charge Balance		-1.6	-0.6	-0.8
pН	S.U.	6.37	6.36	6.40
Eh	mV	130	184	302
Alkalinity	mg/L as CaCO <sub>3</sub>	335	415	605
As	mg/L	0.000230	0.000670	0.00840
В	mg/L	0.0854	0.0873	0.120
Ва	mg/L	0.410	0.382	0.443
Са	mg/L	140	131	124
Cd	mg/L	0.000016	0.000016	0.000016
CI	mg/L	32.7	16.6	26.1
Со	mg/L	0.000435	0.000435	0.001000
Cr	mg/L	0.000220	0.000840	0.000083
F	mg/L	0.260	0.330	0.380
Fe	mg/L	16.6	17.3	8.81
K	mg/L	5.33	5.99	9.78
	mg/L	0.0438	0.0402	0.0254
Mg	mg/L	35.6	30.8	43.1
Mn	mg/L	0.716	0.610	1.72
Mo	mg/L	0.000450	0.00240	0.0592
Na	mg/L	10.1	7.02	63.8
P	mg/L-P	0.137	0.134	0.0173
SO <sub>4</sub>	mg/L	169	57.7	16.2
MINERAL PHASES	- Saturation Indices (a)			-
Ferrihydrite	Fe(OH) <sub>3</sub>	3.7	3.7	3.5
Siderite	FeCO <sub>3</sub>	-2.2	-2.1	-1.9
Melanterite	FeSO <sub>4</sub> 7H <sub>2</sub> O	-6.8	-7.3	-7.8
Rhodochrosite	MnCO <sub>3</sub>	-0.9	-0.9	-0.3
Birnessite	MnO <sub>2</sub>	-19.5	-17.8	-13.1
Manganite	MnOOH	-9.2	-8.4	-5.9
Gypsum	CaSO₄:2H₂O	-1.2	-1.7	-2.3
Jarosite-H	(H <sub>3</sub> O)Fe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	1.0	0.2	-1.8
Jarosite-K	KFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	6.9	6.1	4.3
Jarosite-Na	NaFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	3.6	2.6	1.6
Calcite	CaCO <sub>3</sub>	-0.6	-0.5	-0.4
Magnesite	MgCO <sub>3</sub>	-1.8	-1.8	-1.4
Barite	BaSO <sub>4</sub>	1.3	0.8	0.3
Witherite	BaCO <sub>3</sub>	-3.5	-3.4	-3.1
Fluorite	CaF <sub>2</sub>	-2.1	-1.9	-1.8
Carbon Dioxide	pCO <sub>2</sub> (g) (b)	-0.9	-0.8	-0.6

# Notes:

Non-detect values equal 1/2 analytical detection limit Redox converted from field ORP to Eh by +200 mV  $\,$ 

<sup>(a)</sup> Saturation indices between -0.5 and 0.5 identified by bold type and grey shading

### Appendix C: Speciation Modeling

Parameter	Units	S-TP-8D	S-TP-8M	S-TP-8S
Sampling Date		Nov-18	Nov-18	Nov-18
Charge Balance		-1.2	-0.7	1.4
pН	s.u.	6.34	6.37	6.43
Eh	mV	130	136	136
Alkalinity	mg/L as $CaCO_3$	334	356	374
As	mg/L	0.000880	0.000910	0.000430
В	mg/L	0.0659	0.0817	0.0845
Ва	mg/L	0.363	0.248	0.167
Са	mg/L	110	114	112
Cd	mg/L	0.000016	0.000041	0.000085
CI	mg/L	30.6	36.2	28.2
Со	mg/L	0.000435	0.000435	0.000435
Cr	mg/L	0.000360	0.000150	0.000079
F	mg/L	0.260	0.290	0.250
Fe	mg/L	6.67	8.81	0.0120
К	mg/L	3.68	3.81	9.76
Li	mg/L	0.0331	0.0276	0.0183
Mg	mg/L	23.7	25.1	24.4
Mn	mg/L	0.408	0.402	0.594
Мо	mg/L	0.00150	0.00100	0.0166
Na	mg/L	8.33	10.5	28.9
Р	mg/L-P	0.127	0.0750	0.00815
SO <sub>4</sub>	mg/L	32.7	22.0	28.9
MINERAL PHASES	- Saturation Indices (a)			
Ferrihydrite	Fe(OH) <sub>3</sub>	3.3	3.4	0.4
Siderite	FeCO <sub>3</sub>	-1.9	-2.1	-3.2
Melanterite	FeSO₄ 7H₂O	-7.2	-7.6	-8.7
Rhodochrosite	MnCO <sub>3</sub>	-1.1	-1.1	-0.8
Birnessite	MnO <sub>2</sub>	-19.8	-19.5	-19.0
Manganite	MnOOH	-9.5	-9.3	-9.0
Gypsum	CaSO <sub>4</sub> :2H <sub>2</sub> O	-1.9	-2.1	-2.0
Jarosite-H	(H <sub>3</sub> O)Fe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	-1.5	-1.4	-10.6
Jarosite-K	KFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	4.2	4.2	-4.5
Jarosite-Na	NaFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	1.0	1.2	-7.5
Calcite	CaCO <sub>3</sub>	-0.7	-0.6	-0.5
Magnesite	MgCO <sub>3</sub>	-2.0	-1.9	-1.8
Barite	BaSO <sub>4</sub>	0.6	0.2	0.2
Witherite	BaCO <sub>3</sub>	-3.5	-3.6	-3.7
Fluorite	CaF <sub>2</sub>	-2.1	-2.0	-2.2
Carbon Dioxide	pCO <sub>2</sub> (g) (b)	-0.8	-0.8	-0.9

# Notes:

Non-detect values equal 1/2 analytical detection limit Redox converted from field ORP to Eh by +200 mV  $\,$ 

 $^{\rm (a)}$  Saturation indices between -0.5 and 0.5 identified by bold type and grey shading

## Appendix C: Speciation Modeling

Parameter	Units	S-SCPA-2	S-SCPA-3S	S-SCPA-1D
Sampling Date		Jan-18	Jan-18	Jan-18
Charge Balance		0.9	-4.0	-6.3
pН	S.U.	6.86	8.92	8.17
Eh	mV	154	260	5.92
Alkalinity	mg/L as CaCO <sub>3</sub>	219	170	228
As	mg/L	0.00200	0.0720	0.0921
В	mg/L	0.348	67.8	7.68
Ва	mg/L	0.153	0.0329	0.0799
Са	mg/L	73.4	501	101
Cd	mg/L	0.000240	0.00160	0.000440
CI	mg/L	20.5	23.1	25.0
Со	mg/L	0.00180	0.000365	0.000365
Cr	mg/L	0.000420	0.000300	0.000190
F	mg/L	0.220	0.600	1.20
Fe	mg/L	1.35	0.0343	0.779
K	mg/L	4.35	40.1	11.8
	mg/L	0.0167	0.0434	0.0287
Mg	mg/L	20.0	9.60	23.9
Mn	mg/L	0.113	0.0179	0.0979
Mo	mg/L	0.0265	8.07	2.23
Na	mg/L	13.9	58.5	27.0
P	mg/L-P		-	-
	mg/L	48.5	1290	200
MINERAL PHASES	- Saturation Indices (a)		• •	• =
Ferrihydrite	Fe(OH) <sub>3</sub>	1.8	2.6	2.5
Siderite	FeCO <sub>3</sub>	-0.6	-6.2	0.3
Melanterite	FeSO₄ 7H₂O	-6.1	-11.7	-5.8
Rhodochrosite	MnCO <sub>3</sub>	-1.3	-1.2	-0.1
Birnessite	MnO <sub>2</sub>	-17.0	-6.6	-17.3
Manganite	MnOOH	-8.1	-1.2	-6.8
Gypsum	CaSO₄:2H₂O	-1.9	-0.1	-1.2
Jarosite-H	(H <sub>3</sub> O)Fe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	-7.6	-10.8	-9.6
Jarosite-K	KFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	-1.8	-1.8	-1.7
Jarosite-Na	NaFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	-4.7	-5.1	-4.8
Calcite	CaCO₃	-0.4	1.3	0.9
Magnesite	MgCO <sub>3</sub>	-1.7	-1.0	-0.3
Barite	BaSO <sub>4</sub>	0.4	0.8	0.7
Witherite	BaCO <sub>3</sub>	-3.5	-3.1	-2.5
Fluorite	CaF <sub>2</sub>	-2.4	-1.1	-0.9
Carbon Dioxide	pCO <sub>2</sub> (g) (b)	-1.5	-4.4	-2.8

## Notes:

Non-detect values equal 1/2 analytical detection limit Redox converted from field ORP to Eh by +200 mV  $\,$ 

 $^{\rm (a)}$  Saturation indices between -0.5 and 0.5 identified by bold type and grey shading

### Appendix C: Speciation Modeling

Parameter	Units	S-SCPA-3D	
Sampling Date		Jan-18	†
Charge Balance		-7.5	
рН	s.u.	8.16	
Eh	mV	349	†
Alkalinity	mg/L as CaCO <sub>3</sub>	185	†
As	mg/L	0.0912	†
В	mg/L	79.5	]
Ва	mg/L	0.0777	
Са	mg/L	548	
Cd	mg/L	0.00740	
CI	mg/L	27.1	ļ
Со	mg/L	0.000365	
Cr	mg/L	0.000620	
F	mg/L	2.90	
Fe	mg/L	0.138	
K	mg/L	60.3	
Li	mg/L	0.170	
Mg	mg/L	60.2	
Mn	mg/L	0.202	
Mo	mg/L	43.5	
Na	mg/L	116	
Р	mg/L-P	-	
SO <sub>4</sub>	mg/L	1820	
MINERAL PHASES	- Saturation Indices (a)		т
Ferrihydrite	Fe(OH) <sub>3</sub>	2.9	ļ
Siderite	FeCO <sub>3</sub>	-4.8	1
Melanterite	FeSO <sub>4</sub> 7H <sub>2</sub> O	-9.7	ļ
Rhodochrosite	MnCO <sub>3</sub>	-0.4	ļ
Birnessite	MnO <sub>2</sub>	-6.3	
Manganite	MnOOH	-1.0	ļ
Gypsum	CaSO <sub>4</sub> :2H <sub>2</sub> O	0.0	
Jarosite-H	(H <sub>3</sub> O)Fe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	-6.8	
Jarosite-K	KFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	2.3	
Jarosite-Na	NaFe <sub>3</sub> (SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>6</sub>	-1.0	
Calcite	CaCO <sub>3</sub>	1.0	
Magnesite	MgCO <sub>3</sub>	-0.4	
Barite	BaSO <sub>4</sub>	1.4	
Witherite	BaCO <sub>3</sub>	-3.0	
Fluorite	CaF <sub>2</sub>	0.3	ļ
Carbon Dioxide	pCO <sub>2</sub> (g) (b)	-3.1	

#### Notes:

Non-detect values equal 1/2 analytical detection limit Redox converted from field ORP to Eh by +200 mV

 $^{\rm (a)}$  Saturation indices between -0.5 and 0.5 identified by bold type a